## TELEDYNE PHILBRICK PRODUCT GUIDE

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## TELEDYNE PHILBRICK IS

... a perennial pioneer, having invented a good many of the analog techniques that are now in universal use. Since our founding in 1946 as George A. Philbrick Researches, Inc., we have been continually challenged by a few (competent) compet tors and many (imitative) latecomers, but have been able to find renewed strength in the depth of our creative resources. Fortunately that creativity, stimulated by our passionate need to lead, has kept us in the forefront of the industry.

Among the earliest Philbrick products was a series of operational amplifiers which stirred the imagination of the electronics world and pointed the way to the "packaged circuit module" design concept. From the first tube-type amplifiers produced by the company has grown an aston-
ishing proliferation of complex and sophisticated modules encompassing a wide variety of analog and digital circuit functions including the following noteworthy firsts:

- First commercially available op amps.
- First low bias current parametric op amp (patented).
- First hermetically-sealed hybrid chopper stabilized op amp.
- First gated operational amplifier module.
- First temperature compensated log amplifier (patented).
- First low cost, high accuracy Voltage-toFrequency (V/F) and Frequency-toVoltage (F/V) Converters.
- First high-performance "Deglitched" D/A Converter.



## TOTAL CAPABILITY... the key to success

Teledyne Philbrick's engineering, marketing, and manufacturing operations are located in a modern facility just off Route 128 . . . greater Boston's famous "Electronics Row." Operations include manufacturing facilities for discrete component products as well as thin and thick-film hybrid devices. Our facilities have been carefully designed for optimized high quality/ high volume production. All manufacturing operations are constantly monitored by our quality control and engineering departments to ensure strict conformity to performance and reliability criteria. . traditional hallmarks of the Teledyne Philbrick product line.

Throughout Teledyne Philbrick's impressive history, our foremost consideration has been the needs of our customers. Our engineers and scientists are continually pushing state-of-the-art technologies to their practical limits in order to produce products which give complete customer satisfaction, particularly relying on guaranteed performance and ease of application. All Teledyne Philbrick resources (engineering, manufacturing, quality control and marketing) are dedicated to successfully achieving this goal.

## ENGINEERING...the first essential

A competent, professional, goal-oriented team of engineer-scientists working in a creatively stimulating environment is the foundation of Teledyne Philbrick's continuing success. Research, design, production, and application engineers are the product innovators who consistently provide practical, proven solutions to myriad problems within even the most difficult time and cost constraints.

Teledyne Philbrick "Specials"
No standard product line, however broad, can encompass the total spectrum of potential applications. Certain optimized electrical parameters or unusual package
designs are sometimes necessary to meet inflexible customer requirements. Teledyne Philbrick engineers are experienced specialists in evaluating and satisfying unusual requirements.

Outstanding examples of recently developed Teledyne Philbrick "specials" include devices for pollution control, display systems, air traffic control, aircraft ignition systems, fetal heart monitoring, and process control systems.

How can these "special" talents and resources be put to work on your behalf? Let us quote on your requirements.



Photo courtesy of Raytheon FAA Plan View Display

## MANUFACTURING...making it smaller

Teledyne Philbrick excels in the art of miniaturized packaging of high quality products. One technique extensively used to achieve this goal is hybrid packaging.

Teledyne Philbrick's manufacturing capability for the production of hybrid circuit modules is considered by many to be the finest in the industry. We have maintained our position of superiority by seeking out, developing, and implementing the most modern manufacturing methods. Our processes make maximum use of controlled automation to ensure consistent highquality production. We are continually evaluating and evolving hybrid technologies to ensure the highest performance and reliability at the lowest possible prices.


Philbrick's hybrid facility in Dedham, employs the most advanced manufacturing equipment available, some of which was solely conceived and developed at Philbrick, because our exacting technical requirements were beyond the scope of existing equipment suppliers.
One example of Philbrick's internally-designed production hardware is a computized chip tester which will test 500 transistor chips per hour and sort them into 1000 separate categories. This unique matching hardware provides us with exceptional time and cost economies and permits us to more closely control circuit performance.

Philbrick's engineering talent in advanced

thick and thin-film processes is unsurpassed. Constant experimentation and accumulated years of experience have produced proprietary processing techniques that enable us to manufacture products with exceptional repeatability, reliability, and stability.
Skilled labor is a key element in the production of high quality hybrid circuits. To ensure optimum reliability and performance, quality components are assembled by proficient personnel. Their work is constantly checked by quality control inspectors who monitor every stage of production, from incoming inspection to the final appearance. All units, from the simplest to the most sophisticated, are $100 \%$ inspected electrically and mechanically.


## QUALITY CONTROL...enforcing the highest standards

Teledyne Philbrick's well staffed Quality Control Department maintains the rigid standards which protect our well established reputation for products of the highest quality. Every Philbrick production lot is carefully inspected and tested at appropriate stages of the production cycle.

Military, space, and man-life equipment applications, however, require the most stringent quality-insurance quarantees. These high reliability devices are Philbrick's specialty. Military, NASA, or severe commercial qualification tests are routinely performed at Philbrick. Our products have contributed to such high-reliability projects as Apollo, Minuteman, F-4, and others.

HIGH RELIABILITY DISCRETES . . .
Modular (discrete component) linear and data conversion products are manufactured in full compliance with all MIL-SPEC requirements including environmental, parts, materials, and processes with full MIL documentation. Modules have been delivered to the requirements of MIL-E4158, MIL-E-5400, MIL-T-21200 and other specifications and are fully qualified for military system usage. MIL-STD-454 and MIL-STD-701 parts are used including JAN-TX and ER reliability-screened components with full source control and inplant materials control. A Full Configuration Management System insures continued product uniformity, and Quality Assurance Control per MI L-Q-9858 assures complete specification conformance and product reliability.


## HIGH-RELIABILITY MICROCIRCUITS

Many Philbrick Micropackaged linear and data conversion products can be processed to meet the stringent requirements of the following military documents:

MIL-M-38510-General Specifications for Microcircuits
MIL-Q-9858A-Quality Program Requirements
MIL-STD-883-Test Methods and Procedures for Microelectronics
Outlined below are the Teledyne Philbrick Production Processing procedures per method 5004 referencing MIL-STD-883 inspection and test documentation as applicable.

Standard micropackaged linear microcircuits available with optional MIL-TYPE processing include Models Q25AH (page 17), 1412 (page 19), 141410 (page 21). Also available with optional MIL-TYPE processing are Series 1319, 1321, 1322, 1323, 1324, 1339, 1402, 1421, 1422, $1423,1425,1426,1427$, and 1429.

MIL-type micropackaged data-converters are detailed on pages 38 and 39 .

For detailed information on Philbrick's high reliability products send for publication number M-883, which is available by completing the post-paid card at the rear of this catalog or contact factory directly.

MANUFACTURING, SCREENING, AND INSPECTION
FOR "MIL-TYPE" MICROCIRCUITS

| Screen | 883 - Method - 5004, Class B |
| :---: | :---: |
| Internal Visual (Pre-Cap) | 2010 - Test Condition - B |
| Stabilization Bake | $\begin{aligned} & \text { 1008- Test Condition - B } \\ & \left(125^{\circ} \mathrm{C}\right) \end{aligned}$ |
| Temperature Cycling | Method 1010, Test Condition - B $\left(-55 \text { to }+125^{\circ} \mathrm{C}\right)$ |
| Constant Acceleration | ```Method - 2001 Test - Condition - "D" - 20,000 G's Y1 - Only (1)``` |
| Seal <br> a. Fine <br> b. Gross | Method-1014. <br> a. Test Cond. - " $A$ " <br> $P_{E}=5$ Atmospheres (2) <br> $t_{1}=1$ Hour <br> $t_{2}=30$ Minutes <br> Leak - Rate @ $5 \times 10^{-8} \mathrm{cc} / \mathrm{Sec}$ <br> b. Fluorocarbon Gross Leak |
| Burn-In Test | Method - 1015 <br> 168 Hours @ $125^{\circ} \mathrm{C}$ |
| Final Electrical Tests | Per Unit Electrical Specifications |
| External - Visual | Method - 2009 |

## Notes:

1. (a.) 14-Pin Dip Units: Test Cond "B," 10,000 G's
(b.) 24-Pin Dip Units and Model 1412: Test Cond. "'A," 5,000 G's
2. 24-Pin Dip Units and Model 1412: 30 P.S.I:

## MARKETING \& SALES... providing the services you need

No matter where you are located in the world, you may place your order directly with us or through your nearest Philbrick Engineering Representative. (Note: If we do not yet have a representative in your country, please contact us directly). REPRESENTATIVES STOCK AMPLE QUANTITIES OF MANY STANDARD PRODUCTS, THUS CAN OFFER SAMEDAY DELIVERY. Prices listed in this catalog are F.O.B. Factory, Dedham, Massachu setts, U.S.A.; quotations on custom items, quantity orders, and other price information will be furnished by your local representative on request. Quotations are normally valid for thirty days.

To Help Us Process Your Order Quickly
Please specify model numbers and model names. For example: "Model 1427, Microcircuit Operational Amplifier" or "Model 4103, A/D Converter." Be sure to include the prefix or suffix on certain model numbers to identify special versions of the product.

If your purchase order is a confirmation of an advance verbal order, it should be sent to the office where the advance order was placed. All confirmations should be marked "CONFIRMATION ONLY - DO NOT DUPLICATE."

Acknowledgements will be sent out prompt-
ly by us for United States and Canadian orders on Teledyne Philbrick's standard acknowledgement forms.

MODIFICATIONS TO EQUIPMENT Special identification markings and other minor modifications can generally be made available at a slight increase in price and delivery time. Your inquiries and specifications should be directed to your Philbrick Engineering Representative.

## Regarding Shipment of Your Order

Shipments to destinations within the United States are normally made directly from the factory in Dedham, and are billed F.O.B. Dedham, Massachusetts.


Local representatives should be contacted first for small quantity purchases as the required units may be available from their stock. Shipments to other parts of the world are from the local representative's stock or directly from the factory.

## Terms and Conditions of Sale

The minimum order accepted by Philbrick is $\$ 25.00$. On all orders, unless alternative arrangements have been made in advance, payment is due NET 30 DAYS following date of shipment. Foreign payments and terms are arranged on an individual basis by Philbrick's International Sales Department.

## Warranty

Limitation of Liability. Our goods are warranted by us to be free from defects of material or manufacture and to conform to the applicable published ratings and characteristics in effect at the time of shipment. Our liability under such warranty is limited to replacing or repairing, at our option, any goods found to be defective in such respects which are returned to us transportation prepaid within one year from the date of shipment. In no event shall we be liable for collateral or consequential damages. This warranty shall not apply to any goods which have been subjected to misuse, improper installation, repair, alteration, neglect, accident, inundation, fire or operation outside their published maximum ratings. We will have the right of final determination of the cause and existence of any defect under this warranty.

## Repairs or Replacement

In accordance with the conditions of the Warranty Statement, we ask that all apparently out-of-order equipment be returned to us, whether repairable or not, so that what we learn from any units found to have defects may be applied toward product improvements and new product designs.

If for any reason you wish to return equipment to us, please contact the Teledyne Philbrick sales office for a "Return Mater-
ials Authorization Form" before returning the equipment. Written authorization must first be obtained before returning any merchandise. Proceed according to the instructions on the RMA form.

To expedite handling of your equipment, please enclose a copy of a letter stating model number, model name, serial number, date códe, the detailed reason for return, the applications circuit diagram (if possible), any applicable purchase order number, and your exact return address. The original of that letter should be addressed to Sales Department, Teledyne Philbrick, Allied Drive at Route 128, Dedham, Massachusetts 02026.

If any Philbrick unit requiring repair or replacement is a critical component or is part of a System requiring minimum down-time, please notify your Philbrick Engineering Representative immediately. He is often able to arrange for the loan of a temporary replacement unit.

## Data Sheets

Each product manufactured by Philbrick is described in depth on an individual technical bulletin which includes electrical performance, physical and mechanical specifications, as well as descriptive data and circuit diagrams for employment of the device in typical applications.
With each shipment of equipment, a complete set of technical data is enclosed.

## Applications Bulletins

Concise, informal sheets released periodically to illustrate salient, useful, and often new applications.

## Short Form Supplementary Catalogs

Useful, comparative summaries of product families can be found in short form catalogs. They will be made available between catalog release dates, for all new instrumentation developed by Philbrick.

NOTE: the reply cards at the back of this catalog may be used to request specific literature and add your name to our mailing list if you wish.


## NEW PRODUCTS FROM TELEDYNE PHILBRICK



## 4050

MICROCIRCUIT D/A CONVERTERS

- 8/10/12-bit Resolution
- $0.8 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Nonlinearity T.C.
- -55 to $+125^{\circ} \mathrm{C}$ Temp. Range
- $2 \mu$ s Settling Time to $1 / 2$ LSB
- Voltage or Current Output
- Hermetically Sealed
- Complete and Self-Contained
- Feature Philbrick's Proprietary Quad Switch
- Precision Voltage Source
- Test Equipment
- Display Systems


## 3420

## MONOLITHIC CURRENT

## QUAD SWITCH

- 16-bit Accuracy
- $0.5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Nonlinearity T.C.
- 30 nSec Settling to Within 0.01\%
- 3 nSec Switching Speed
- Low Leakage
- Operates over +5 to $\pm 15 \mathrm{~V}$
- ICBO of 6 pA
- D/A and A/D Converters
- Meter Drive
- x-y Recorders
- Programmable Voltage Sources



## 4253 and 425301

## LOW DRIFT FET

## INSTRUMENTATION AMPLIFIERS

- Ultra High $Z_{\text {in }}-10^{13} \Omega$
- Low Drift - $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, Max.
- High CMRR -110 db min. to 100 Hz
- Low Noise $-2 \mu \mathrm{~V}$ p.p
- Low Bias Current -10 pA, Max.
- Adj. Gain, 1 - 5000
- Low Level Instrumentation
- High Resolution Control Loops
- High Impedance Sensors
- Pressure Transducers
- Bridge Amplifiers
- Biomedical Engineering


4853
HIGH SPEED SAMPLE-HOLD AMPLIFIER

- $1 \mu$ s Acquisition Time to $0.01 \%$ max.
- 300 nsec Settling Time to $0.01 \%$
- 20 kHz Bandwidth
- 0.005\% Linearity
- 1 mV maximum Feedthrough
- $\pm 1 \mathrm{nSec}$ max. Aperature Uncertainty Time
- Data Acquisition Systems
- A/D Converters
- D/A Converters
- Deglitch Circuits


## 4028 and 4029, 8 and 10 bit MULTIPLYING D/A CONVERTERS

- Settling Time: $3 \mu \mathrm{Sec}$
- Feedthrough: -60 dB @ 10 kHz
- Reference $\pm 10 \mathrm{~V} @ 80 \mathrm{kHz}$
- Gain TC $\pm 25 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- PSRR $\pm 0.002 \% / \% \Delta V_{S}$
- CRT Character Display
- Variable Gain Amplifier
- Vector Generation
- Digital to Synchro Conversion
- Test Systems

4701, 4703, and 4705
FREQUENCY-TO-VOLTAGE CONVERTERS
470147034705

- F.S. Output 10 kHz $100 \mathrm{kHz} \quad 1 \mathrm{MHz}$
- Resolution $>13$-bits $>13$-bits $>13$-bits
- Linearity 0.008\% 0.015\% 0.02\%
- Stability,
$\mathrm{ppm} /{ }^{\circ} \mathrm{C} \quad \pm 27 \quad \pm 44 \quad \pm 47$
- High Noise Rejection
- DTL/T $T^{2}$ L output; 10 -load fanout
- Remote control or monitoring
- 2-wire digital transmission
- Electronic testing
- Magnettic tape recording
- Telemetering
- Isolation
- Servo loops
- Arithmetic operations
- Synchronous speed control


4702 and 4704
FREQUENCY-TO-VOLTAGE CONVERTERS

47024704

- F.S. Input 10 kHz 100 kHz for 10 V out
-Linearity 0.008\% 0.006\%
- Accept DTL/T $T^{2}$ L, HNIL, Sine

Square or Triangular Wave Inputs

- Adjustable Hysterisis for use with small signals
- 20 mA Output Rating
- Magnetic Pickups
- Optical Pickups
- Phase Locked Loops
- Telemetry Systems
- Frequency Monitors
- Remote Data Transmission
- Tachometers
- Flow Meters
- Broadband FM Discriminators
- Doppler Sonar \& Radar
- Frequency vs. Amplitude X-Y Plots


1324/1427
FAST SETTLING MICROCIRCUITS

## 1324

- Fast Settling - $1 \mu \mathrm{~s}$ to $0.01 \%$
- Low $\mathrm{E}_{\mathrm{OS}} \mathrm{TC}-15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ (132401)
- Pin compatible with 715 types
- Latch-up proof
- Fast Settling Amplifiers \& Buffers
- 12-bit Digital-to-Analog Converters
- High Speed Multiplexer Amplifiers
- Current-to-Voltage Conversion
- Data Converter Deglitchers 1427
- Fast Settling - $1.5 \mu$ s to $0.01 \%$
- Hermetically Sealed - Meets Mil Std 883
- Fully Differential FET
- Low Bias Current
- Data Converters
- Sample-and-Hold
- Precision Integrators
- Pulse Amplifiers
- Charge Amplifiers


## 1420 SERIES

## FET MICROCIRCUITS

- 1421 General Purpose, Economy High CMRR/Low Bias Current
- 1422 Economy Wideband 5 MHz GBW/15 pA Ibias
- 1423 Low Voltage Drift $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \mathrm{E}_{\text {OS }} \mathrm{TC} /-10 \mathrm{pA}$ Ibias
- 1424 Lowest Price FET $6 \mathrm{~V} / \mu \mathrm{s}$ Slew Rate/50 pA Ibias
- 1425 Low Bias Current $5 \mathrm{pA} \mathrm{I}_{\text {bias }} / 1 \mathrm{mV} \mathrm{E}_{\mathrm{OS}}$
- 1426 Low Voltage Drift $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C} \mathrm{E}_{\text {OS }} \mathrm{TC} / 1 \mathrm{mV} \mathrm{E}_{\text {OS }}$
- 1427 - Fast Settling
- 1428 Economy "Micro Module"

Herm Seal/5 pA Ibias

- 1429 Ultra-Low Bias Current $0.25 \mathrm{pA} \mathrm{I}_{\text {bias }} / 1 \mathrm{mV} \mathrm{E}_{\mathrm{os}}$


4454 and 4455

## PRECISION MULTIPLIERS/DIVIDERS <br> 44544455

- High Accuracy 0.5\% 0.25\%
- 50 kHz full Power Bandwidth
- 5 mA Output Current
- $0.01 \% /{ }^{\circ} \mathrm{C}$ Scale Factor T.C. max. (4455)
- Short Circuit Protection

4456 and 4457
WIDEBAND MULTIPLIERS/DIVIDERS
44564457

- High Accuracy 1\% 0.5\%
- Wide Bandwidth 5 MHz dB power; 1 MHz full power freq.
- $1 \%$ max. Phase Shift at 300 kHz
- 10 mA Output Current

4112, 4113, 4114 ECONOMY A/D CONVERTERS

- High Speed: <60 $\mu$ s for 12 -bits
- High Stability: $\pm 20 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Unipolar \& Bipolar Input
- Serial \& Parallel Output
- Data Acquisition Systems
- Test \& Measuring Equipment
- Telemetering Systems

4024, 4025, 4026, 4027 ECONOMY D/A CONVERTERS

- 12-bit Resolution
- 200 ns Settling Time
- BCD - 4026, 4027
- Voltage or Current Output
- TTL/DTL Compatible
- Internal Reference
- Display Systems
- Test Equipment
- Instrumentation


## Operational Amplifier Classification

To aid in the selection of the proper amplifier, we have classified both discrete and microcircuit amplifiers into groups according to their salient specifications and most common applications. The group explanations below list the factors which determine the amplifier classification. Cross references for amplifiers considered to be in more than one category are listed with the group specifications.
For those applications where only a micropackage will suffice, we have listed the specifications for FET microcircuits on pages 24-25 and bipolar microcircuits on pages 26-27.

## GROUP I - GENERAL PURPOSE -

 MODERATE PERFORMANCE (Pages 14-15)Amplifiers in this group are best suited where moderate specifications of voltage drift, current drift, input impedance, and bandwidth are acceptable. The voltage drift range will be from $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ to $30 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ and current drift in the range of $0.2 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ to $3 \mathrm{nA} /{ }^{\circ} \mathrm{C}$. Typical numbers for bandwidth are 1 MHz to 2 MHz and frequency for full output of 10 kHz to 20 kHz . Applications for this group are general, such as inverters, followers as impedance buffers, adders, or amplifiers to be used with non-linear modules.

## GROUP II - LOW BIAS CURRENT, HIGH INPUT IMPEDANCE (Pages 16-17)

FET input amplifiers and parametric (varactor bridge) amplifiers generally appear in this classification. The amplifiers in this group are best suited for impedance levels above 100 $k \Omega$. The high input impedance reduces loading errors due to source resistance and the low leakage currents at the inputs provide for minimum error referred to the output. Applications include integrators, electometers, current to voltage converters, sample and hold amplifiers and low level logarithmic amplifiers. Parametric amplifiers such as the 1702 and 170201 are the ultimate in low bias current op-amps. They will resolve signal levels as low as $10^{-15}$ amps with source impedance levels up to $10^{14} \Omega$, and are best suited to measure low frequency, low level signals in such applications as electrometers and seismograph amplifiers.

## GROUP III - LOW VOLTAGE DRIFT (Pages 18-19)

Amplifiers in this group have the lowest voltage drift due to changes in time, temperature, and power supply variation. The temperature coefficient will be in the range of $0.1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ to $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, with the lowest temperature coefficients appearing in the chopper-stabilized amplifiers. Applications for this group are where low level signals are to be resolved or amplified, such as low level signal conditioning and low level comparators.

GROUP IV - WIDEBAND, FAST RESPONSE (Pages 20-21)
Important specifications for amplifiers in this class are gainbandwidth product, frequency for full output, slewing rate, settling time, and overload recovery. Amplifiers in this group have a unity gain bandwidth of greater than 10 MHz . Applications include high speed A-D and D-A conversion, sample-and-hold circuits, and high speed comparators.

GROUP V - SPECIAL PURPOSE (Pages 22-23)
Special purpose amplifiers include low power drain (micropower, battery operated) wide supply voltage range; high voltage, and high output current types. Individual data sheets show specific applications.

## MICROCIRCUITS

## FET Input

These low priced, high reliability amplifiers are designed for high impedance applications where low error currents are important. This comprehensive line will optimize most circuit designs with a minimum of effort. All units are pin compatible with the popular 741 amplifier types and require no additional stabilizing networks. The complete line of FET microcircuits is listed on pages 24 and 25 as well as individually specified under the main group headings.

## BIPOLAR Input

These amplifiers have the low cost and high reliability of the 741 types plus high performance. For optimizing new designs, or updating old ones, these units are the perfect choice. Specifications are listed under the major headings, and collectively on pages 26-27.


# Selecting Operational Amplifiers by Salient Parameter 

Often times the selection of the right amplifier means studying many columns of data to choose the right combination of specifications to suit a particular application. To make the selection process easier we have listed in the reference chart below Philbrick's high performance amplifier's according to their optimized parameters. If more relaxed specification are acceptable, check those amplifiers detailed under the broader categories of General Purpose, Low Bias Current, Low Drift, Wideband, or special purpose detailed on the following pages.

DISCRETE MODELS
MICROCIRCUIT MODELS

| OUTPUT <br> RANGE | Voltage, $\geqslant 20 \mathrm{~V}$ |  | 1005, 1022, 1034 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Current, $\geqslant 30 \mathrm{~mA}$ |  | 1008, 1016, 1017, 1025 |  |
| GAIN | Rated load, $\geqslant 200 \mathrm{k}$ |  | 1020, 1022, 1028, 1700, 1701, 1703 | 1323, 1412 |
| FREQUENCY RESPONSE (Inverting) | Small signal (unity gain, open loop), $\geqslant 10 \mathrm{MHz}$ |  | 1025, 1027, 1030, 1700 | 1317, 1321, 1322, 1324, 141410 |
|  | Large signal: full output $\geqslant 500 \mathrm{kHz}$ |  | 1016, 1025, 1027, 1030, 1700 | 1321, 1322, 141410 |
|  | Slew rate $\geqslant 50 \mathrm{~V} / \mu \mathrm{Sec}$ |  | 1016, 1025, 1027, 1030, 1700 | 1322, 141410 |
|  | Settling time $\leqslant 1.5 \mu \mathrm{Sec}$ to $0.01 \%$ |  | 1025, 1027, 1030 | 1321, 1322, 1324, 1427, 141410 |
| INPUT VOLTAGE RANGE | Common mode (dc linear operation), $\geqslant 20 \mathrm{~V}$ |  | SP2A, 1005, 1016, 1022, 1034, 1702 | 1402 |
|  | Differential (between inputs), $\geqslant 40 \mathrm{~V}$ |  | 1005, 1016, 1022, 1702 | 1402 |
|  | Common mode rejection ratio (dc) $\geqslant 100,000$ |  | SP2A, 1016, 1020, 1021, 1022, 1023, 1702 | 1319, 1321, 1323, 1324, 1423 |
| INPUT VOLTAGE OFFSET | Initial (without external trim) $\leqslant 2 \mathrm{mV}$ |  | 1020, 1022, 1023, 1700, 1701, 1703 | 140201, 1412, 1423, 1425, 1426, 1427, 1428, 1429 |
|  | Vs. Temperature $\leqslant 5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |  | 1020, 1023, 1700, 1701, 1703 | 1319, 1412, 1423, 1426 |
|  | Vs. Time $\leqslant 25 \mu \mathrm{~V} /$ day |  | 1020, 1700, 1701, 1703 | 1319, 1412, 1426 |
|  | Vs. Power supply $\leqslant 10 \mu \mathrm{~V} / \mathrm{V}$ |  | 1016, 1022, 1700, 1701, 1702, 1703 | 1319, 1323, 1324, 1412, 1423 |
| INPUT <br> BIAS CURRENT | Initial $\leqslant 1 \mathrm{pA}$ |  | SP2A, 1029, 1702 | 1429 |
|  | Vs. Temperature $\leqslant 3 \mathrm{pA} /{ }^{\circ} \mathrm{C}$ slope @ $25^{\circ} \mathrm{C}$ |  | SP2A, 1021, 1023, 1029, 1700, 1702, 1703 | 1402, 1425, 1429 |
|  | Vs. Power Supply |  | SP2A, 102 1, 1022, 1029, 1700, 1701, 1702, 1703 | 1402, 1421, 1422, 1425, 1426, 1428, 1429 |
|  | Vs. Time |  | SP2A, 1029, 1700, 1701, 1702, 1703 | 1402, 1429 |
|  | Difference (tracking) |  | SP2A, 1021, 1023, 1026, 1029, 1702 | 1425, 1429 |
| INPUT IMPEDANCE | Differential $\geqslant 10^{12} \Omega$ |  | SP2A, 1021, 1023, 1029, 1702 | 1402, 1429 |
|  | Common mode $\geqslant 10^{12} \Omega$ |  | SP2A, 1021, 1023, 1029, 1702 | 1423, 1427, 1429, 141410 |
| NOISE <br> (Referred to input) | $\begin{aligned} & \text { Flicker } \\ & (0.016 \text { to } 1.6 \mathrm{~Hz}) \end{aligned}$ | Voltage p-p $\leqslant 1 \mu \mathrm{~V}$ | SP2A, 1020, 1021, 1023, 1028, 1034, 1700, 1701, 1703 | 1319, 1421, 1426, 140410 |
|  |  | Current p-p $\leqslant 0.2 \mathrm{pA}$ | SP2A, 1006, 1021, 1023, 1025, 1029, 1030, 1702 | 1402, 1429 |
|  | Midband$(1.6 \text { to } 160 \mathrm{~Hz})$ | Voltage rms $\leqslant 1 \mu \mathrm{~V}$ | SP2A, 1017, 1025, 1030, 1700, 1703 | 1319, 1321, 1322, 140410 |
|  |  | Current rms $\leqslant 0.2 \mathrm{pA}$ | SP2A, 1006, 1025, 1029, 1030, 1702 | 1422, 1429 |
|  | Broadband ( 160 Hz to 16 kHz ) | Voltage rms $\leqslant 1 \mu \mathrm{~V}$ | 1005, 1016, 1017 | 1319, 1321, 1322, 140410 |
|  |  | Current rms $\leqslant 2 \mathrm{pA}$ | 1022, 1026, 1029 | 1402, 1429 |
| POWER REQUIREMENT | Voltage range |  | 1006, 1022, 1034 | 1323, 1402, 140410 |
|  | Current: quiescent $\leqslant 1 \mathrm{~mA}$ |  | 1006 | 1323, 1402, 140410 |
| TEMPERATURE. | Operating ( $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ ) |  |  | 131901, 132102, 132201, 132302, Q25AH |

## Groupl. General Purpose



1. $R_{L L}=2 \mathrm{k} \Omega$
2. Settling time to $0.01 \%$, typical
3. At a gain of $100,4.2 \mathrm{~V} / \mu \mathrm{Sec}$ at $\mathrm{A}=1$
4. Offset vs. temperature
5. Voltage rms ( 10 Hz to 10 kHz )
6. GBW @ $A=100$

* Socket not supplied by Teledyne Philbrick.

Other amplifiers suitable for this category are:
MODEL PAGE
102616
103422
131926

## MICROCIRCUIT

| 1424 <br> FET, Economy | $\begin{gathered} 1428 \\ 142801 \\ 142802 \\ \text { FET, Economy } \\ \text { Micromodule } \end{gathered}$ |  |  | $\begin{gathered} 1319 \\ 131901 \\ \text { High Performance } \\ \text { Low Drift } \end{gathered}$ |  | $\begin{gathered} 1339 \\ 133901 \\ 133902 \\ \text { General Purpose } \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ |  |  | $\pm 10 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  |  |
| $\pm 5 \mathrm{~mA}$ | $\pm 5 \mathrm{~mA}$ |  |  | $\pm 5 \mathrm{~mA}$ |  | $\pm 5$ | 10 | 10 mA |
| 20,000 | 100,000 |  |  | 50,000 |  | 15 | 40 | 50 k |
| 1 MHz | 1 MHz |  |  | 1 MHz (typ.) |  | 100 MHz (typ.) © |  |  |
| 70 kHz (typ.) | 35 kHz (typ.) |  |  | 8 kHz |  | 350 kHz (typ.) (3) |  |  |
| 100 kHz (typ.) | 50 kHz |  |  | 10 kHz (typ.) |  | 500 kHz (typ.) (3) |  |  |
| $6 \mathrm{~V} / \mu \mathrm{Sec}$ | $3 \mathrm{~V} / \mu \mathrm{Sec}$ |  |  | $0.6 \mathrm{~V} / \mu \mathrm{Sec}$ (typ.) |  | $34 \mathrm{~V} / \mu \mathrm{Sec}$ (3) |  |  |
| $3 \mu \mathrm{Sec}$ (2) | $3 \mu \mathrm{Sec}{ }^{(2)}$ |  |  | -- |  | -- |  |  |
| $\pm 10 \mathrm{~V}$ | $\pm 12 \mathrm{~V}$ |  |  | $\pm 12 \mathrm{~V}$ |  | $\pm 11 \mathrm{~V}$ |  |  |
| $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ |  |  | $\pm 15 \mathrm{~V}$ |  | $\pm 15 \mathrm{~V}$ |  |  |
| 3,200 | 4 | 4 | 10 k | 100,000 (typ.) |  | 10,000 |  |  |
| $\pm 50 \mathrm{mV}$ | $\pm 2$ | 1 | 1 mV | $\pm 5$ | $2 \mu \mathrm{~V}$ | $\pm 7.5$ | 7.5 | 3 mV |
| $10 \mathrm{k} \Omega$ pot | -- |  |  | $10 \mathrm{k} \Omega$ pot |  | $100 \mathrm{k} \Omega$ pot |  |  |
| $75 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 50$ |  | $25 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 25$ | $15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 12$ | 5 | $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| $\pm 50 \mu \mathrm{~V}$ | $\pm 25 \mu \mathrm{~V}$ |  |  | $\pm 5 \mu \mathrm{~V}$ |  | $\pm 10 \mu \mathrm{~V}$ |  |  |
| $\pm 150 \mu \mathrm{~V} / \mathrm{V}$ | $\pm 100 \mu \mathrm{~V} / \mathrm{V}$ |  |  | $\pm 10 \mu \mathrm{~V} / \mathrm{V}$ |  | $\pm 30 \mu \mathrm{~V} / \mathrm{V}$ |  |  |
| 50 pA | -25 | 10 | 5 pA | $+250$ | $+50 \mathrm{nA}$ | +1 | 0.6 | $0.5 \mu \mathrm{~A}$ |
| doubles ea. $+10^{\circ} \mathrm{C}$ | doubles ea. $+10^{\circ} \mathrm{C}$ |  |  | $\pm 30 \mathrm{pA} /{ }^{\circ} \mathrm{C} \text { typ. }$ |  | $\pm 200 \mathrm{pA} /{ }^{\circ} \mathrm{C}$ |  |  |
| $\pm 2 \mathrm{pA} / \mathrm{V}$ | $\pm 1 \mathrm{pA} / \mathrm{V}$ |  |  | -- |  |  |  |  |
| $\pm 2 \mathrm{pA}$ | $\pm 1 \mathrm{pA}$ |  |  | -- |  | $\pm 25 \mathrm{nA}$ |  |  |
| $\pm 0.5 \mathrm{pA}$ | $\pm 10$ | 5 | 2 pA | $\pm 3$ 2 nA |  | $\pm 20 \mathrm{nA}$ |  |  |
| $10^{12} \\| 2 \mathrm{pF}$ | $10^{12} \\| 3 \mathrm{pF}$ |  |  | $2 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $300 \mathrm{k} \Omega$ |  |  |
| $10^{12} \\| 2 \mathrm{pF}$ | $10^{12} \\| 3 \mathrm{pF}$ |  |  | $100 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $40 \mathrm{M} \Omega$ |  |  |
| $3 \mu \mathrm{~V}$ | $3 \mu \mathrm{~V}$ |  |  | -- |  | -- |  |  |
| 0.3 pA | 0.3 pA |  |  | -- |  | -- |  |  |
| $2 \mu \mathrm{~V}$ | $2 \mu \mathrm{~V}$ |  |  | -- |  | -- |  |  |
| 0.3 pA | 0.3 pA |  |  | -- |  | -- |  |  |
| $3 \mu \mathrm{~V}$ | $3 \mu \mathrm{~V}$ |  |  | $1 \mu \mathrm{~V}$ (3) |  | $2 \mu \mathrm{~V}$ (5) |  |  |
| 0.1 pA | 0.1 pA |  |  | -- |  | -- |  |  |
| $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ | $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ |  |  | $\pm 15 \mathrm{~V}( \pm 6$ to $\pm 22 \mathrm{~V})$ |  | $\pm 15 \mathrm{~V}( \pm 9$ to $+18 \mathrm{~V})$ |  |  |
| $\pm 6 \mathrm{~mA}( \pm 11 \mathrm{~mA})$ | $\pm 5 \mathrm{~mA}( \pm 10 \mathrm{~mA})$ |  |  | $\pm 3 \mathrm{~mA}( \pm 8 \mathrm{~mA})$ |  | $\pm 7 \mathrm{~mA}( \pm 12 / 17 / 17 \mathrm{~mA})$ |  |  |
| 0 to +70 | -25 to +85 |  |  | $0 \text { to }+70$ |  | $0 \text { to }+70$ |  |  |
| -65 to +150 | $-65 \text { to }+150$ |  |  | $-65 \text { to }+150$ |  | $-65 \text { to }+150$ |  |  |
| TO-99 | T2 |  |  | TO-99 |  | TO-99 |  |  |
| * | 6035 |  |  | * |  | * |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

Selected versions are available on all models, consult factory.
Specifications listed left to right correspond to model numbers top to bottom above.

## Group 2. Low Bias Current/High Input Impedance

DISCRETE


1. Settling time to $0.01 \%$, typical.
2. $10 \mu \mathrm{~V}$ rms typical ( 1 Hz to 100 Hz )
3. $G \times B W @ A=100$

* Socket not supplied by Teledyne Philbrick

Other amplifiers suitable for this category are

| MODEL | PAGE | MODEL | PAGE |
| :--- | :--- | :--- | :--- |
| 1021 | 16 | 1423 | 25 |
| 1023 | 18 | 1424 | 15 |
| 1025 | 20 | 1426 | 25 |
| 1027 | 20 | 1427 | 25 |
| 1030 | 20 | 1428 | 24 |
| 1421 | 24 | 1700 | 19 |
| 1422 | 25 | 1701 | 19 |
|  |  | 1703 | 19 |


| Econ | $\begin{gathered} 1702 \\ 170201 \end{gathered}$ <br> ifferential my Parametric | $\begin{gathered} 1425 \\ 142501 \\ 142502 \\ \text { FET } \\ \text { Low Bias Current } \end{gathered}$ |  |  | $\begin{gathered} 1429 \\ 142901 \\ 142902 \\ \text { FET Ultra Low Bias } \end{gathered}$ |  |  | Q25AH FET High Reliability (Premium) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm 10 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  |  | $\pm 10 \mathrm{~V}$ |  |  | $\pm 11 \mathrm{~V}$ |
| $\pm 5 \mathrm{~mA}$ |  | $\pm 5 \mathrm{~mA}$ |  |  | $\pm 5 \mathrm{~mA}$ |  |  | $\pm 2.2 \mathrm{~mA}$ |
| 100,000 |  | 100,000 |  |  | 20 | 40 | 40 k | 20,000 |
| 1 kHz |  | 1 MHz |  |  | 500 kHz |  |  | 30 MHz |
| 40 Hz |  | 35 kHz (typ.) |  |  | 35 kHz (typ.) |  |  | 100 kHz (3) |
| 50 Hz |  | 50 kHz |  |  | 50 kHz |  |  | 167 kHz |
| $2.5 \mathrm{~V} / \mathrm{ms}$ |  | $3 \mathrm{~V} / \mu \mathrm{Sec}$ |  |  | $3 \mathrm{~V} / \mu \mathrm{Sec}$ |  |  | $8 \mathrm{~V} / \mu \mathrm{Sec}$ |
| -- |  | $3 \mu \mathrm{Sec}$ |  |  | $5 \mu \mathrm{Sec}$ |  |  | -- |
| $\pm 100 \mathrm{~V}$ |  | $\pm 12 \mathrm{~V}$ |  |  | $\pm 10 \mathrm{~V}$ |  |  | $\pm 10 \mathrm{~V}$ |
| $\pm 200 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  |  | $\pm 15 \mathrm{~V}$ |  |  | $\pm 15 \mathrm{~V}$ |
| 100,000 |  | 10,000 |  |  | 10,000 |  |  | 5,000 |
| $\pm 5 \mathrm{mV}$ |  | $\pm 2$ | 1 | 1 mV | $\pm 2$ | 1 | 2 mV | $\pm 10 \mathrm{mV}$ |
| $50 \mathrm{k} \Omega$ pot |  | $10 \mathrm{k} \Omega$ pot |  |  | $10 \mathrm{k} \Omega$ pot |  |  | $250 \mathrm{k} \Omega$ |
| $\pm 30$ | $10 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 50$ | 25 | $10 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 90$ | 30 | $60 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 55 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| $\pm 20 \mu \mathrm{~V}$ |  | $\pm 25 \mu \mathrm{~V}$ |  |  | $\pm 10 \mu \mathrm{~V}$ |  |  | $\pm 50 \mu \mathrm{~V}$ |
| $\pm 20 \mu \mathrm{~V} / \mathrm{V}$ |  | $\pm 100 \mu \mathrm{~V} / \mathrm{V}$ |  |  | $\pm 100 \mu \mathrm{~V} / \mathrm{V}$ |  |  | $\pm 70 \mu \mathrm{~V} / \mathrm{V}$ |
| $\pm 0.005 \mathrm{pA}$ |  | -10 | -5 | $-5 \mathrm{pA}$ | -1 | -0.5 | $-0.25 \mathrm{pA}$ | -150 pA |
| $\pm 0.0002 \mathrm{pA} /{ }^{\circ} \mathrm{C}$ |  | doubles ea $+10^{\circ} \mathrm{C}$ |  |  | doubles ea. $+10^{\circ} \mathrm{C}$ |  |  | doubles ea. $+10^{\circ} \mathrm{C}$ |
| $\pm 0.0005 \mathrm{pA} / \mathrm{V}$ |  | $\pm 1 \mathrm{pA} / \mathrm{V}$ |  |  | $\pm 1 \mathrm{pA} / \mathrm{V}$ |  |  | $\pm 10 \mathrm{pA} / \mathrm{V}$ |
| $\pm 0.001 \mathrm{pA}$ |  |  |  |  | $\pm 1 \mathrm{pA}$ |  |  | $\pm 3 \mathrm{pA}$ |
| $\pm 0.003 \mathrm{pA}$ |  | $\pm 1 \mathrm{pA}$$\pm 5$ |  |  | $\pm 0.3$ | 0.1 | 0.1 pA | $\pm 10 \mathrm{pA}$ |
| $3 \times 10^{11} \Omega \\| 15 \mathrm{pF}$ |  | $10^{12} \Omega \\| 3 \mathrm{pF}$ |  |  | $10^{13} \Omega \\| 3 \mathrm{pF}$ |  |  | $10^{11} \Omega$ |
| $10^{14} \Omega$ |  | $10^{12} \Omega \\| 3 \mathrm{pF}$ |  |  | $10^{13} \Omega \\| 3 \mathrm{pF}$ |  |  | $10^{11} \Omega$ |
| $10 \mu \mathrm{~V}$ (2) |  | $3 \mu \mathrm{~V}$ |  |  | $2.8 \mu \mathrm{~V}$ |  |  | $5 \mu \mathrm{~V}$ |
| -- |  | 0.3 pA |  |  | 0.04 pA |  |  | 0.2 pA |
| $10 \mu \mathrm{~V}$ |  | $2 \mu \mathrm{~V}$ |  |  | $2.9 \mu \mathrm{~V}$ |  |  | $2 \mu \mathrm{~V}$ |
| -- |  | 0.3 pA |  |  | 0.05 pA |  |  | 1 pA |
| $200 \mu \mathrm{~V}$ |  | $3 \mu \mathrm{~V}$ |  |  | $4.8 \mu \mathrm{~V}$ |  |  | $2 \mu \mathrm{~V}$ |
| -- |  | 0.1 pA |  |  | $0.03 \mathrm{pA}$ |  |  | 3 pA |
| $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ |  | $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ |  |  | $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ |  |  | $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ |
| $+13,-8 \mathrm{~mA}(+18,-13 \mathrm{~mA})$ |  | $\pm 2.8 \mathrm{~mA}( \pm 7.8 \mathrm{~mA})$ |  |  | $\pm 5 \mathrm{~mA}( \pm 10 \mathrm{~mA})$ |  |  | $\pm 7.6 \mathrm{~mA}( \pm 9.8 \mathrm{~mA})$ |
| 0 to +70 |  | -25 to +85 |  |  | 0 to +70 |  |  | -55 to +125 |
| -55 to +125 |  | -55 to +150 |  |  | -65 to +150 |  |  | -62 to +150 |
| E5 |  | TO-99 |  |  | TO-99 |  |  | TO-8 |
| NSK-20 |  | * |  |  | * |  |  | US-Q |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

Selected versions are available on all models, consult factory.
Specifications listed left to right correspond to model numbers top to bottom above.

# Group 3. Low Voltage Drift 



1. Settling time to $0.01 \%$, typical.
2. With external trim resistor supplied
3. $\pm 1 \mathrm{pA} /{ }^{\circ} \mathrm{C}, \max .\left(0\right.$ to $\left.+60^{\circ} \mathrm{C}\right)$
4. Offset vis. temperature
5. Voltage rms ( 10 Hz to 10 kHz )

* Socket not supplied by Teledyne Philbrick

| $\begin{array}{r} 17 \\ 17 \\ \text { Ge } \\ \text { Purpose } \end{array}$ | 01 <br> 101 <br> eral Chopper | $\begin{gathered} 1703 \\ 170301 \end{gathered}$ <br> Economy Chopper |  | $\begin{gathered} 1426 \\ 142601 \\ 142602 \\ 142603 \\ \text { FET, Low Drift } \end{gathered}$ |  |  |  | $\begin{gathered} 1423 \\ 142301 \\ 142302 \\ \text { FET, Low Drift } \end{gathered}$ |  |  | $\begin{gathered} 1319 \\ 131901 \end{gathered}$ <br> Premium Low Drift |  | 1412 <br> Mini Chopper Stabilized Microcircuit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm 12 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  |  |  | $\pm 10 \mathrm{~V}$ |  |  | $\pm 10 \mathrm{~V}$ |  |  |
|  |  | $\pm 5 \mathrm{~mA}$ |  |  |  |  |  |  |  |  |  |  | $\pm 5 \mathrm{~mA}$ |
| $10^{7}$ |  |  |  | 100,000 |  |  |  | 100,000 |  |  | 50,000 |  | $10^{6}$ |
| 1 MHz | typ.) | 1 MHz (typ.) |  |  |  |  |  | 3 MHz (typ.) |  |  | $1 \mathrm{MHz} \text { (typ.) }$ |  | $1 \mathrm{MHz} \text { (typ.) }$ |
| 20 kHz |  | 4.5 kHz |  | 35 kHz (typ.) |  |  |  | $70 \text { kHz (typ.) }$ |  |  | $8 \mathrm{kHz}$ |  | $14 \mathrm{kHz}$ |
| 30 kHz |  | $7 \text { kHz (typ.) }$ |  | 50 kHz |  |  |  | 100 kHz |  |  | 10 kHz (typ.) |  | $20 \mathrm{kHz}$ |
| $1.2 \mathrm{~V} / \mathrm{\mu}$ |  | $0.25 \mathrm{~V} / \mu \mathrm{Sec}$ |  | $3 \mathrm{~V} / \mu \mathrm{Sec}$ |  |  |  | $6 \mathrm{~V} / \mu \mathrm{Sec}$ |  |  | $0.6 \mathrm{~V} / \mu \mathrm{Sec} \text { (typ.) }$ |  | $1.2 \mathrm{~V} / \mu \mathrm{Sec}(\mathrm{min}$. |
| -- |  | -- |  | $3 \mu \mathrm{Sec}$ |  |  |  | $10 \mu \mathrm{Sec}$ |  |  |  |  | $--$ |
| -- |  |  |  | $\pm 12 \mathrm{~V}$ |  |  |  | $\pm 10 \mathrm{~V}$ |  |  | $\pm 12 \mathrm{~V}$ |  | $--$ |
| -- |  |  |  | $\pm 15 \mathrm{~V}$ |  |  |  | $\pm 15 \mathrm{~V}$ |  |  | $\pm 15 \mathrm{~V}$ |  | -- |
| -- |  | -- |  | 4 10 10 10 k |  |  |  | 100,000 |  |  | 100,000 (typ.) |  |  |
| $\pm 15 \mu \mathrm{~V}$ |  |  | $15 \mu \mathrm{~V}$ | $\pm 2$ | 1 | 1 | 1 mV | $\pm 2$ | 1 | $1 \mu \mathrm{~V}$ | $\begin{array}{l\|l}  \pm 5 & 2 \mu \mathrm{~V} \\ \hline \end{array}$ |  | $\pm 25 \mu \mathrm{~V}$ |
| $50 \mathrm{k} \Omega$ |  | $50 \mathrm{k} \Omega$ pot |  | $10 \mathrm{k} \Omega \text { pot }$ |  |  |  | $1 \mathrm{k} \Omega$ pot |  |  | $10 \mathrm{k} \Omega$ pot |  | $50 \mathrm{k} \Omega \text { pot }$ |
| $\pm 0.25$ | $0.1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 1{ }_{ \pm} \pm 0.3 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |  | $\begin{aligned} & \pm 50 \\ & \pm\end{aligned} 25\|10\| 5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |  |  |  | $\pm 5$ | 2 | $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 25$ 15 $\mu$ |  | $\pm 0.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| $\pm 5 \mu \mathrm{~V} /$ |  | $\pm 5 \mu \mathrm{~V} / \mathrm{yr}$ |  | $\pm 10 \mu \mathrm{~V}$ |  |  |  | $\pm 10 \mu \mathrm{~V}$ |  |  | $\pm 5 \mu \mathrm{~V}$ |  | $\pm 1 \mu \mathrm{~V} / \mathrm{mo}$ |
| $\pm 0.2 \mathrm{pV} / \mathrm{V}$ |  | $\pm 1 \mu \mathrm{~V} / \mathrm{V}$ |  | $\pm 100 \mu \mathrm{~V} / \mathrm{V}$ |  |  |  | $\pm 10 \mu \mathrm{~V} / \mathrm{V}$ |  |  | $\pm 10 \mu \mathrm{~V} / \mathrm{V}$ |  | $\pm 0.25 \mu \mathrm{~V} / \mathrm{V}$ |
| $\pm 50 \mathrm{pA}$ |  |  |  | doubles ea. $+10^{\circ} \mathrm{C}$ |  |  |  | $-10 \mathrm{pA}$ |  |  | +250$\pm 30 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ typ. (4) |  | $\pm 100 \mathrm{pA}$ |
| $\pm 1 \mathrm{pA} /$ |  | $\pm 2 \quad 0.5 \mathrm{pA} /{ }^{\circ} \mathrm{C}$ |  |  |  |  |  | doubles ea. $+10^{\circ} \mathrm{C}$ |  |  |  |  | $\pm 5 \mathrm{pA} /{ }^{\circ} \mathrm{C}$ |
| $\pm 2 \mathrm{pA} /$ |  | $\pm 5 \mathrm{pA} / \mathrm{V}$ |  | $\pm 1 \mathrm{pA} / \mathrm{V}$ |  |  |  | $\pm 5 \mathrm{pA} / \mathrm{V}$ |  |  | -- |  | $\pm 3 \mathrm{pA} / \mathrm{V}$ |
| $\pm 10 \mathrm{pA}$ |  | $\pm 10 \mathrm{pA} / \mathrm{yr}$ |  | $\pm 1 \mathrm{pA}$ |  |  |  | $\pm 1 \mathrm{pA}$ |  |  | -- |  | $\pm 1 \mathrm{pA} / \mathrm{mo}$ |
| -- |  | -- |  | $\begin{array}{l\|l\|l\|l}  \pm 10 & 5 & 10 & 10 \mathrm{pA} \\ \hline \end{array}$ |  |  |  | $\pm 2 \mathrm{pA}$ |  |  | $\pm 3 \mathrm{2nA}$ |  | -- |
| $500 \mathrm{k} \Omega$ | $\\| 100 \mathrm{pF}$ | $800 \mathrm{k} \Omega \\| 100 \mathrm{pF}$ |  | $10^{\prime 1} \Omega \\| 3 \mathrm{pF}$ |  |  |  | $10^{12} \Omega \\| 3 \mathrm{pF}$ |  |  | $2 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $500 \mathrm{k} \Omega \\| 100 \mathrm{pF}$ |
| -- |  | -- |  | $10^{12} \Omega \\| 3 \mathrm{pF}$ |  |  |  | $10^{12} \Omega \\| 3 \mathrm{pF}$ |  |  | $100 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | -- |
| $1 \mu \mathrm{~V}$ |  | $1 \mu \mathrm{~V}$ |  | $4 \mu \mathrm{~V}$ |  |  |  | $5 \mu \mathrm{~V}$ |  |  | -- |  | $5 \mu \mathrm{~V}$ |
| 5 pA |  | 3 pA |  | $0.5 \mathrm{pA}$ |  |  |  | 0.2 |  |  | -- |  | 4 pA |
| $2 \mu \mathrm{~V}$ |  | $2 \mu \mathrm{~V}$ |  | $2 \mu \mathrm{~V}$ |  |  |  | $2 \mu \mathrm{~V}$ |  |  | -- |  | $5 \mu \mathrm{~V}$ |
| 5 pA |  | 6 pA |  | $0.5 \mathrm{pA}$ |  |  |  | 0.3 |  |  | -- |  | 5 pA |
| $5 \mu \mathrm{~V}$ |  | $2 \mu \mathrm{~V}$ |  | $3 \mu \mathrm{~V}$ |  |  |  | $3 \mu \mathrm{~V}$ |  |  | $1 \mu \mathrm{~V} \text { © }$ |  | $7 \mu \mathrm{~V}$ |
| 25 pA |  | -- |  | 0.2 pA |  |  |  | 2 pA |  |  | -- |  | 30 pA |
| $\pm 15 \mathrm{~V}( \pm 8$ to $\pm 20 \mathrm{~V})$ |  | $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18)$ |  | $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ |  |  |  | $\pm 15 \mathrm{~V}( \pm 12$ to $\pm 18 \mathrm{~V})$ |  |  | $\pm 15 \mathrm{~V}( \pm 6 \text { to } \pm 22 \mathrm{~V})$ |  | $\pm 15 \mathrm{~V}( \pm 8$ to $\pm 20 \mathrm{~V})$ |
| $\pm 3 \mathrm{~mA}( \pm 8 \mathrm{~mA})$ |  | $\pm 5 \mathrm{~mA}( \pm 10 \mathrm{~mA})$ |  | $\pm 2.8 \mathrm{~mA}( \pm 7.8 \mathrm{~mA})$ |  |  |  | $\pm 10 \mathrm{~mA}( \pm 15 \mathrm{~mA})$ |  |  | $\pm 3 \mathrm{~mA}( \pm 8 \mathrm{~mA})$ |  | $+3,-5 \mathrm{~mA}( \pm 8 \mathrm{~mA})$ |
| -25 to +85 |  | 0 to +70 |  | -25 to +85 |  |  |  | 0 to +70 |  |  | $0 \text { to }+70$ |  | -25 to +85 |
| -55 to +125 |  | -55 to +125 |  | -65 to +150 |  |  |  | $-55$ | $\text { to }+$ | $125$ | $-65 \text { to }+150$ |  | -55 to +125 |
| E5 |  | E11 |  | TO-99 |  |  |  | S4 |  |  | TO-99 |  | A5 |
| NSK-20 |  | NSK-20 |  | * |  |  |  | * |  |  | * |  | 6053 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Selected versions are available on all models, consult factory.
Specifications typical at $25^{\circ} \mathrm{C}$ with nominal power supply, unless otherwise indicated.
Specifications typical at $25^{\circ} \mathrm{C}$ with nominal power
supply, unless otherwise indicated.


1. 75 nsec to $0.1 \%$ max.
2. 5 pF negative input to common
3. Compensated for unity gain
4. For 5 Hz to 50 kHz bandwidth, $\mathrm{e}_{\mathrm{n}}=6 \mu \mathrm{~V} \mathrm{rms}$, typical
5. This socket not supplied by Teledyne Philbrick, available from Barnes Corp., Lansdowne, Pa.
6. Gain $\times$ Bandwidth @ $A_{C l}=5$
7. Gain $\times$ Bandwidth @ $A_{c l}=10$
8. Offset vs. temperature
9. Voltage rms $(10 \mathrm{~Hz}$ to kHz$)$
10. 500 nsec to $0.1 \%$
11. 300 nsec to $0.1 \%$
12. Also available in 14 pin DIP, as the Model 132410. Consult factory.
13. $R_{L L}=2 \mathrm{k} \Omega$
14. With $499 \Omega, 1 \% \mathrm{MF}$
15. Inverting or non-inverting

Socket not supplied by Teledyne Philbrick


Another amplifier suitable for this category is: MODEL PAGE
$1700 \quad 18$

Selected versions are available on all models, consult factory.
Specifications listed left to right correspond to model numbers top to bottom above.

## Group 5. Special Purpose

## DISCRETE



1. $E_{o}= \pm 100 \mathrm{~V}$
2. Inverting mode only. $\mathrm{f}_{\mathrm{S}}=10 \mathrm{kHz}$ and slew rate $=1.2 \mathrm{~V} / \mu \mathrm{Sec}$ for noninverting mode.
3. Short circuit $= \pm 80 \mathrm{~mA}$
4. Offset vs. temperature
5. Voltage rms ( 10 Hz to 10 kHz )
6. When inputs are less than 5 mV apart. When inputs are more than 50 mV apart quiescent current is $\pm 3 \mathrm{~mA}$.

* Socket available from Barnes Corp., Lansdowne, Pa. Not available from Teledyne Philbrick.


Selected versions are available on all models, consult factory.
Specifications listed left to right correspond to model numbers top to bottom above.

## FET Microcircuits



1. $R_{L L}=2 \mathrm{k} \Omega$
2. Settling time to $0.01 \%$ max.
3. Gain $\times$ Bandwidth @ $A_{c l}=5$
4. $e_{\mathrm{n}}=4.2 \mu \mathrm{~V}$ rms typical from 5 Hz to 50 kHz
5. $A_{c l}=5$

* Socket not supplied by Teledyne Philbrick.


Selected versions are available on all models, consult factory.

Specifications listed left to right correspond to model numbers top to bottom above.

## Bipolar Microcircuits

GENERAL LOW
PURPOSE
DRIFT

| 1339 | 1319 |  |
| :---: | :---: | :---: |
| 133901 | 131901 |  |
| 133902 | High Performance | 1317 |
| General Purpose | Low Drift | Wideband |


0. $G B W @ A=100$

1. $@ A=100,4.2 \mathrm{~V} / \mu \mathrm{Sec} @ A=1$
2. $G \times B W @ A=10, f_{t}=10 \mathrm{MHz} @ A=1$ (typ.)
3. $3.5 \mu \mathrm{Sec}$ to $0.01 \%$
4. $G \times B W @ A=10$
5. $3 \mu \mathrm{Sec}$ to $0.01 \%$
6. 5 Hz to 50 kHz
7. When inputs are less than 5 mV apart. When inputs are more than 50 mV apart quiescent current is $\pm 3 \mathrm{~mA}$ typical.
8. $G \times B W @ A=100$
9. $@ A=100$
10. @ $A=5$
11. $\mathrm{R}_{1}=220 \Omega, \mathrm{C}_{1}=22 \mathrm{pF}$, NOISE Gain $=1$
12. Inverting or non-inverting
13. Noise Gain $=2, \mathrm{R}_{1}=220 \Omega, \mathrm{C}_{1}=15 \mathrm{pF}$

Socket not supplied by Teledyne Philbrick

| $1321$ $132101$ <br> Wideband High Input Impedance |  | $\begin{gathered} 1322 \\ 132201 \\ \text { High Slew Rate } \end{gathered}$ |  | $\begin{gathered} 1324 \\ 132401 \\ \text { Fast Settling } \end{gathered}$ |  | $\begin{gathered} 1323 \\ 132301 \\ 132302 \\ \text { Low Power } \\ \text { General Purpose } \end{gathered}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm 10 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  | $\pm 12 \mathrm{~V}$ |  |  |
| $\pm 10 \mathrm{~mA}$ |  | $\pm 10 \mathrm{~mA}$ |  | $\pm 10 \mathrm{~mA}$ |  | $\pm 10 \mathrm{~mA}$ |  |  |
| 80,000 |  | 7,500 |  | 100,000 |  | 200,000 |  |  |
| 100 MHz (typ.) ${ }^{(2)}$ |  | 20 MHz (typ.) (1) |  | 8 MHz (1) (1) |  | 1 MHz (typ.) |  |  |
| 320 kHz (0) |  | 1.2 MHz (0) |  | 350 kHz (11) (13) |  | 25 kHz (typ.) |  |  |
| $35 \mathrm{~V} / \mu \mathrm{Sec}$ (0) |  | $120 \mathrm{~V} / \mu \mathrm{Sec}$ (0) |  | $35 \mathrm{~V} / \mu \mathrm{Sec}$ (11) (1) |  | $20 \mathrm{~V} / \mu \mathrm{Sec}$ |  |  |
| $500 \mathrm{nSec} \text { (3) }$ |  | $300 \mathrm{nSec}$ |  | $1.0 \mu \mathrm{Sec} \text { (12) (1) }$ |  | $10 \mu \mathrm{Sec}$ |  |  |
| $\pm 12 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |  | $\pm 11 \mathrm{~V}$ |  |  |
| $\pm 15 \mathrm{~V}$ |  |  |  | $\pm 15 \mathrm{~V}$ |  |  |  |  |
| 100,000 |  | 30,000 |  |  |  | 200,000 |  |  |
| $\pm 5 \mathrm{mV}$ |  | $\pm 10 \mathrm{mV}$ |  |  |  | $\pm 5$ 3 3 mV |  |  |
| $100 \mathrm{k} \Omega$ pot |  | $20 \mathrm{k} \Omega$ pot |  | $50 \mathrm{k} \Omega \text { pot }$ |  |  |  |  |
| $\pm 20 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |  | $\pm 15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |  | $\pm 30$ | $15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ (max.) | $1 \mathrm{M} \Omega$ pot$\pm 10 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |  |  |
| $30 \mu \mathrm{~V} / \mathrm{V}$ |  | $30 \mu \mathrm{~V} / \mathrm{V}$ |  | $10 \mu \mathrm{~V} / \mathrm{V}$ |  |  |  |  |
| $\pm 25 \mathrm{nA}$ |  | $\pm 250 \mathrm{nA}$ |  | +300 200 nA |  | $\begin{array}{\|l\|l\|l\|} \hline \pm 40 & 20 & 20 \mathrm{nA} \\ \hline \end{array}$ |  |  |
| 5 nA |  | $20 \mathrm{nA}$ |  | 50 | $35 \mathrm{nA}$ | $2.5 \mathrm{nA}$ |  |  |
| $0.8 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ |  | $\pm 0.5 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ |  | $\pm 0.3 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ |  | $0.5 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ |  |  |
| $300 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $100 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $3 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $2 \mathrm{M} \\| 3 \mathrm{pF}$ |  |  |
| $1000 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $1000 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $1000 \mathrm{M} \Omega \\| 3 \mathrm{pF}$ |  | $200 \mathrm{M} \\| 3 \mathrm{pF}$ |  |  |
| $1 \mu \mathrm{~V}$ |  | $1 \mu \mathrm{~V}$ |  | $6 \mu \mathrm{~V}$ |  | $10 \mu \mathrm{~V}$ |  |  |
| $\pm 15 \mathrm{~V}( \pm 8$ to $\pm 22 \mathrm{~V})$ |  | $\pm 15 \mathrm{~V}( \pm 8$ to $\pm 20 \mathrm{~V})$ |  | $\pm 15 \mathrm{~V}( \pm 12 \text { to } \pm 18 \mathrm{~V})$ |  | $\pm 15 \mathrm{~V}( \pm 5.5 \text { to } \pm 20 \mathrm{~V})$ |  |  |
| $\pm 4 \mathrm{~mA}( \pm 14 \mathrm{~mA})$ |  | $\pm 6 \mathrm{~mA}( \pm 16 \mathrm{~mA})$ |  | $\pm 15 \mathrm{~mA}( \pm 25 \mathrm{~mA})$ |  | $\pm 80 \mu \mathrm{~A} \text { © }$ |  |  |
| 0 to 70 | -55 to +125 | 0 to 70 | -55 to +125 | $0 \text { to } 70$ |  | 0 to 70 | -25 to +85 | -55 to +125 |
| $-65 \text { to }+150$ |  | -65 to +150 |  | $-65 \text { to }+125$ |  | -65 to +150 |  |  |
| TO-99 |  | TO-99 |  | TO-10 |  | TO-99 |  |  |
| * |  | * |  | * |  | * |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |

Selected versions are available on all models, consult factory
Specifications listed left to right correspond to model numbers top to bottom above.


## Instrumentation Amplifiers



## FEATURES

- Ultra High $Z_{\text {in }}-10^{13} \Omega$
- Very Low Drift - $1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ max.
- High CMRR - $116 \mathrm{~dB} \min$. to 100 Hz
- Low Noise - $2 \mu \mathrm{~V}$ p-p flicker
- Low Bias Current - 10 pA max.
- Single Resistor Gain Selection
- Sense Terminal for Current Feedback
- $\pm 10$ V Output Offsetting Capability
- Small Size, Low Profile $-2 \times 2 \times 0.4^{\prime \prime}$


## APPLICATIONS

- Low Level Instrumentation
- High Resolution Control Loops
- High Impedance Sensors
- Pressure Transducers
- Bridge Amplifiers
- Biomedical Engineering

MODELS 4253 and 425301
Philbrick's high-performance FET Instrumentation Amplifiers, Models 4253 and 425301, are specifically designed to extract and accurately amplify small differential signals from large common mode voltages. A unique bootstrapped FET input circuit provides a very high input impedance to minimize source-loading errors even from very high source impedances. Computer testing and matching of active devices plus the use of precision passive components ensures extreme stability with time and temperature, and provides very low input noise. Functional trimming is used during manufacture to guarantee excellent Common Mode Rejection for both ac and dc signals, even with large source unbalances.

The gain range is adjustable between 1 and 5000 by one external resistor, excellent linearity being maintained throughout this range. The circuit design also includes a provision for offsetting the output by up to $\pm 10$ volts, and features output short circuit protection. Reliable performance even in severe vibration environments is ensured by low profile epoxy encapsulation.


MODELS 4251 and 4252
These instrumentation amplifiers feature extended frequency response and a gain range of 1 to 1000 programmable with a single resistor. Offset voltage is externally adjustable to zero. An output sense terminal allows the amplifier feedback to be taken precisely at the load point. AAnother feature is the CMRR adjust terminal, which allows external trimming of the common mode rejection ratio at the exact gain and frequency desired. This terminal also serves as a reference point for the amplifier output, and output offsets of up to $\pm 10$ volts can be introduced.

|  | $\begin{aligned} & 4251 \\ & 4252 \\ & \text { leband Bipolar } \end{aligned}$ | $\begin{gathered} 4253 \\ 425301 \end{gathered}$ <br> Low-Drift FET |
| :---: | :---: | :---: |
| GAIN |  |  |
| Gain Range (Adj. with Ext. Res.) | 1-1000 | 1-5000 |
| Gain Programming | $A=1+\frac{20 \mathrm{k} \Omega}{\mathrm{R}}$ | $1+\frac{100 \mathrm{k} \Omega}{R_{G}}$ |
| Gain dc Nonlinearity, Max. | $\pm 0.01 \%$ | $\pm 0.005 \%$ |
| Gain dc Nonlinearity vs. Temp. $(A=100)$ | $10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | $30 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| INPUT CHARACTERISTICS |  |  |
| Input Impedance - Differential | $50 \mathrm{M} \Omega$ | $10^{13} \Omega$ |
| Input Impedance - Com. Mode Min. | $30 \mathrm{M} \Omega$ | $10^{13} \Omega$ |
| Input Voltage Range, Min. | $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ |
| OFFSETS AND NOISE |  |  |
| Input Offset Voltage (RTI) Gain $=1000$ | $\pm 3 \mathrm{mV}$ | $\pm 1 \mathrm{mV}$ |
| Input Voltage Offset 425301 | - | $500 \mu \mathrm{~V}$ |
| Input Voltage Offset vs. Temp. G = 1000 | $\pm 2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | $\pm 2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| Input Voltage Offset vs. Temp. 425301 | - | $\pm 1 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| Input Bias Current | 30 nA | $-10 \mathrm{pA}$ |
| Input Bias Current vs. Temp., Max. | $\pm 3 \mathrm{nA} /{ }^{\circ} \mathrm{C}$ | $2 \times 10^{\circ} \mathrm{C}$ |
| COMMON MODE REJECTION ( dc - 100 Hz ) |  |  |
| $A=10$, Balanced Source, Min. | 80 dB | 82 dB |
| $A=10$, Balanced Source, Min. 425301 | - | 92 dB |
| $A=1000$, Balanced Source | 110 dB | 114 dB |
| $A=1000$, Balanced Source 425301 |  | 120 dB |
| FREQUENCY RESPONSE |  |  |
| Small Signal $A=100, \pm 1 \%$ Accuracy, Min. | 25 kHz | 500 Hz |
| OUTPUT CHARACTERISTICS |  |  |
| Rated Output Voltage, Min. | $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ |
| Rated Output Current, Min. 4251 | $\pm 100 \mathrm{~mA}$ | $\pm 5 \mathrm{~mA}$ |
| Rated Output Current, Min. 4252 | $\pm 5 \mathrm{~mA}$ | - |
| POWER SUPPLY REQUIREMENTS |  |  |
| Supply Voltage, Rated | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ |
| Supply Current, Quiescent, Max. | $\pm 15 \mathrm{~mA}$ | $\pm 16 \mathrm{~mA}$ |
| TEMPERATURE RANGE (Degrees C ) |  |  |
| Operating, Rated Specs | -25 to +85 | 0 to +50 |
| Storage | -55 to +100 | -55 to +125 |

Typical performance curves for 4253 Series.




## APPLICATION NOTE:

Recommended grounding and shielding practices for instrumentation amplifiers:
a. Ensure that the data acquisition system has a stable ground.
b. Ground the signal circuit at one point only.
c. Signal cable shields should not be used to carry signal currents; they should be connected to ground at only one point, preferably at the signal source.
d. If the signal source operates off ground at some common mode voltage, the signal cable shield should not be grounded; it should be connected to the cen-ter-tap or the "low" side of the signal source.

## Booster Amplifiers



By definition, a Booster is a power amplifier. A current booster is used when the output current is too small to drive the necessary load. Voltage boosters are also available to extend output voltage capabilities of the standard 10 Volt operational amplifier. (See OSPB-100/10)
Because the booster is normally connected inside the operational amplifier's negative feedback loop, its contribution to drift, linearity, and gain error is negligible.

$\qquad$

| mode voltage capability of the amplitier. |  | BQ-100 | 2001 | OSPB-100/10 |
| :---: | :---: | :---: | :---: | :---: |
| OUTPUT | Voltage, min. | $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ | $\pm 100 \mathrm{~V}$ |
|  | Current, min. | 100 mA | 500 mA | $1.5 \mathrm{~mA}(10 \mathrm{~mA}) *$ |
| VOLTAGE GAIN (DC open loop) | At rated load, min. | 0.95 | 0.90 | 19 |
|  | Current gain, min. | 2000 | 40,000 |  |
| FREQUENCY RESPONSE | Full output (no distort.) min. | 400 kHz | 80 kHz | 10 kHz |
|  | Rate limit | $35 \mathrm{~V} / \mu \mathrm{Sec}$ | $10 \mathrm{~V} / \mu \mathrm{Sec}$ | $7 \mathrm{~V} / \mu \mathrm{Sec}$ |
| INPUT VOLTAGE OFFSET | Initial @ $25{ }^{\circ} \mathrm{C}$ | $\pm 0.3 \mathrm{~V}$ | $\pm 0.3 \mathrm{~V}$ | $\pm 0.1 \mathrm{~V}$ |
| INPUT IMPEDANCE | Pos. or neg. input to common | $600 \mathrm{k} \Omega$ | $1 \mathrm{M} \Omega$ | $1 \mathrm{M} \Omega$ |
| OUTPUT IMPEDANCE | Output to common | $3 \Omega$ | $1 \Omega$ | $500 \Omega$ |
| POWER REQUIREMENTS | Nominal supply voltage | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 120 \mathrm{~V}$ |
|  | Voltage range | $\pm 12$ to $\pm 16 \mathrm{~V}$ | $\pm 12$ to $\pm 16 \mathrm{~V}$ | $\pm 100$ to $\pm 125 \mathrm{~V}$ |
|  | Current (quiescent), max. | $\pm 15 \mathrm{~mA}$ | $\pm 50 \mathrm{~mA}$ | $\pm 3.5 \mathrm{~mA}$ |
|  | (full load), max. | $\pm 120 \mathrm{~mA}$ | $\pm 550 \mathrm{~mA}$ | $\pm 6 \mathrm{~mA}( \pm 15 \mathrm{~mA}) *$ |
| CASE STYLE \& SOCKET | Operating | -25 to +85 | -25 to +65 | -25 to +85 |
|  | Storage | -55 to +100 | -55 to +100 | -55 to +85 |
|  |  | AS2, NSK-20 | G1, NSK-9 | SP, QS-15 |

$\qquad$
$\qquad$
*Specifications shown in parenthesis apply when external boost resistors are used. See OSPB-100/10 data sheet.

## Operational Manifold

Teledyne Philbrick Model 5001 Operational Manifold provides the capability of simulating small analog systems and performing computations using plug-in Function Boards that accept many types of operational amplifiers as well as linear and non-linear function modules. The Model 5001's versatility proves invaluable for applications requiring varied types of computing elements.
In addition to its dynamic breadboard characteristics, the Model 5001 is an outstanding educational tool for learning analog theory and circuit design from the basics through complex analog computation and control.
Each Function Board provides a socket for the active operator, and a logical patch field for connecting active and passive elements and interfacing associated circuitry.
The patch field greatly reduces breadboarding time normally required for testing applications. When used for teaching purposes the patch field makes a lucid, easy-to-follow circuit.
The Model 5001 incorporates a built-in regulated dual power supply. The regulated voltages are brought out to Function Board jacks for use as input or reference voltages.

Circuit wiring and interface is performed using standard banana plug patch cables, shorting bars, and plug-in passive and active elements. External signals and output indicators are connected in the same manner.
The Model 5001 is available as a bench model or in a standard, 19 inch rack model. A complete line of accessories is available which includes a variety of Function Boards, hardware kits, and component kits.

## ACCESSORIES

## MODEL 6048 FUNCTION BOARDS

This Function Board accepts the standard 7 or 9 pin " $Q^{\prime}$ " package operational amplifiers. The patch field for interconnecting operational elements includes jacks for external trim, $\pm 15 \mathrm{Vdc}$ regulated, signal ground and power ground.
MODEL 6042 FUNCTION BOARD
This Function Board accepts integrated circuit operational amplifiers similar to 709's or 741's in TO-99 packages.

The patch field includes jacks for external trim, damping networks, $\pm 15 \mathrm{Vdc}$ regulated, signal grounds and power ground.

## MODEL 6049 FUNCTION BOARD

This version accepts our Model 4850 Three-Mode Integrator. Model 6049 is a double size board and comes supplied with the Model 4850 . See pages 58 and 59 for specifications on Model 4850.

## MODEL 6054 FUNCTION BOARD

This Function Board accepts Philbrick Models 4350 and 4351 Log Modules and provides an output proportional to the log or antilog of the input signal. Either a Model 4350 or 4351 is supplied with this double-size function board (specify). See page 52 for 4350/4351 specifications.

## MODEL MAK-2F CONNECTION HARDWARE KIT

 The MAK-2F Hardware Kit includes4 shielded twin tip cables,
12 single tip patch cords,
32 twin tip plugs (for component mounting) and
15 twin tip shorting plugs
MODEL CCK-MF COMPUTING COMPONENT KIT
The CCK-MF Kit includes the following components mounted on twin tip banana plugs.

4 Diodes 1N914
2 Zener Diodes $9.5 \mathrm{~V}, 5 \%$
40 resistors, and
12 capacitors
SPECIFICATIONS

INPUT VOLTAGE

POWER SUPPLY
Output Voltage
Output Current
Regulation to line
Regulation to load
Ripple and Noise
Complete protection against shorts for an indefinite period.
DIMENSIONS $\quad 17^{\prime \prime} \mathrm{L} \times 12^{\prime \prime} \mathrm{W} \times 7.75^{\prime \prime} \mathrm{H}$
WEIGHT
NO. CHANNELS
$115 \mathrm{~V} \pm 10 \%$ (5001) $230 \mathrm{~V} \pm 10 \%$ (5001-01) $50-400 \mathrm{~Hz}$
$\pm 15( \pm 0.15) \mathrm{Vdc}$ $\pm 100 \mathrm{~mA} \mathrm{~min}$. $\pm 0.03 \%$ max. $\pm 0.03 \%$ max. 1.0 mV rms

6 lbs (without Function Boards) 6 single boards or 3 double boards

ORDERING INFORMATION
Model 5001 (specify bench or rack model) (5001-01 for 230 V) (Does not include function boards. Order separately as listed below).
Model 6042 Function Board (less operator) Model 6048 Function Board (less operator)
Model 6049 Function Board (Model 4850 Three Mode Integrator supplied)
Model 6054 Function Board (Model 4350 or 4351 Log Module supplied - please specify)
MAK-2F Connection Hardware Kit
CCK-MF Computing Component Kit

## DATA CONVERSION PRODUCTS

Philbrick manufactures a comprehensive line of data conversion products with an outstanding range of performance characteristics. Reinforced by the reliability, quality, and experienced applications support you expect from Philbrick, these data conversion products are ideally suited for optimiz ing future designs or upgrading present ones.

## ANALOG/DIGITAL CONVERTERS

Philbrick A/D Converters are self-contained, low-profile modules utilizing integration, modified successive approximation, or tracking circuit techniques to provide the right price/performance combination for a wide variety of applications. Proprietary design techniques and the use of high quality components assure adjustment-free operation over the operating temperature range. A feature of Philbrick A/D's allows the user to select single (from external command) or repetitive operation for digital display. Other key features include

- $10 \mu \mathrm{Sec}$ conversion time for 12 -bits (4106)
- Excellent PSRR to $\pm 0.001 \% / \% \Delta \mathrm{~V}$ s
- Relative accuracy $\pm 1 / 2$ LSB maximum ( $\pm 1 / 4$ LSB max. model 4110)
- BCD output (models 4111 and 411110)
- DTL/TTL compatible
- Continuous Tracking and converting (model 4110)


## DIGITAL/ANALOG CONVERTERS

Philbrick D/A converter modules are self-contained, lowprofile units accepting 8 to 14 -bit digital inputs and providing either a voltage or current output. With built-in reference, high speed switching, and a fast settling amplifier in voltage models, each amplifier is fully specified to minimize application difficulties and designed for long-term accuracy and reliability.

- Linearity $\pm 1 / 4$ LSB , typical ( $\pm 1 / 4$ LSB max. on 4050 Series)
- DTL/TTL compatible
- Buffered inputs on high performance models
- 100 ns Settling Time to $0.01 \%$ (models 4014,4016 )
- Excellent PSRR to $\pm 0.002 \% / \% \Delta \mathrm{~V}$ s
- Low Cost: $\$ 19$ (1-9 qty. models 4020,4021 )
- Microcircuit - Hermetically sealed manufactured to MIL-STD-883 (4050 Series)
- Multiplying (models 4028 and 4029)

D/A Converters used in display systems, control systems, and other demanding applications must have good accuracy and resolution; slew and settle quickly; exhibit a high degree of linearity; have extremely low noise and no glitches. For such requirements Philbrick offers the models 4015,4017 , and 4002. Each is actually a small system within a card-mounted module utilizing a unique current-stabilized, non-saturating switching concept to preserve linearity and stability at high speed and eliminate switching transients.

If high performance over a wide temperature range is needed, the 4050 Series of microcircuit D/A Converters is recommended. These units are packaged in a hermetically sealed double D.I.P. and can be processed to MIL-STD-883 to ensure high reliability in military or rugged industrial applications.

A key data conversion accessory is Philbrick's new model 4853, a high-speed sample-hold amplifier for precision applications. This sophisticated module is particularly well suited for use with A/D Converters (particularly successive approximation) and multiplexers in high through-put 12 -bit data-acquisition systems.
A new monolithic quad current switch, Model 3420, is also featured in this section. Philbrick has combined a special topographical design with high quality PNP transistors to achieve higher speeds and greater accuracy than previously possible. Use the Model 3420 to design higher performance $D / A$ and $A / D$ Converters at lower cost.

## D/A \& A/D PARAMETER DEFINITIONS

RESOLUTION: The relative value of the Least Significant Bit (LSB) - the smallest value of change that can be distinguished by an A/D Converter or generated by a D/A Converter. Resolution is determined by Full Scale $/ 2^{n}$ for a converter with " n " binary bits or Full Scale/10 d for a BCD Converter with " $d$ " decimal digits.
For an n-bit converter
A.) Number of steps:
1.) Binary: $2^{n}-1$
2.) $\mathrm{BCD}: 10^{\mathrm{d}}-1$
B.) Value of Smallest step (LSB)

LSB $=$ Full Scale $/ 2^{\text {n }}$
C.) MSB (most significant bit) $=$ Full Scale/2
D.) Full Scale is unreachable by 1 LSB

For example, a 12 -bit converter has an LSB of 0.0244\% of Full Scale. With a Full Scale voltage of 10 V the maximum output voltage is $10.00000 \mathrm{~V}-0.00244 \mathrm{~V}$ or 9.99756 V .

ABSOLUTE ACCURACY: Absolute accuracy for a Converter is defined as the degree to which the actual inputoutput relationship matches the ideal calculated relationship.

RELATIVE ACCURACY: The relative accuracy of a converter is determined by its linearity, and does not include its Scale Factor (gain) and Offset errors. After its Gain and Offset errors are adjusted, a converter with perfect relative accuracy will display perfect absolute accuracy.

SCALE FACTOR ERROR (GAIN ERROR): The difference in slope between the actual input-output relationship and the ideal relationship. This is quoted in percent error of value, ignoring offset error. Normally, this error is easily adjusted out in system calibration.

OFFSET ERROR: The degree to which the transfer function fails to pass through the origin normally measured on the analog axis. If this error is not adjusted to zero, a constant absolute accuracy error is obtained at every point on the transfer function. Offset error does not degrade the relative accuracy.


SCALE FACTOR \& OFFSET ERROR

ADC OFFSET MEASUREMENT: Because of quantization the actual offset of an ADC cannot be measured directly and must be calculated from another measurement or set of measurements. Normally, to plot the transfer function of an ADC, we would measure the analog inputs that result in transitions on the digital output. Since the first transition would ideally occur at $+1 / 2$ LSB, the discrepancy of this first transition is sometimes considered to be the offset error. Each transition, however, is permitted to have offset, scale factor, and linearity errors. Thus another way to measure ADC offset is to extrapolate to zero the best straight line drawn through several lower transitions.

NONLINEARITY: Nonlinearity is the maximum deviation from a straight line drawn between the end points of the input/output transfer function. Nonlinearity is normally specified as some fraction of an LSB. For example, a specification $\pm 1 / 2$ LSB requires the sum of either the positive errors or the negative errors of the individual bits not to exceed $1 / 2$ LSB.


DIFFERENTIAL NONLINEARITY: Differential Nonlinearity describes the difference between the actual analog transition and the calculated value of the LSB over the full digital range. For example, differential nonlinearity of $\pm 1 / 2$ LSB demands that each step be 1 LSB $\pm 1 / 2$ LSB. A differential nonlinearity of $\leqslant 1$ LSB is the maximum allowed for monotonic operation.

MONOTONICITY: A converter is monotonic when it is continuously increasing in response, and each successive level is equal to or greater than the previous one. Monotonicity requires differential nonlinearity to be $\leqslant 1$ LSB.


NONMONOTONIC TRANSFER FUNCTION
QUANTIZING ERROR: The inherent uncertainty of $\pm 1 / 2$ LSB associated with the finite resolution of the digitizing process in ADC's. This uncertainty is the finite scientific rounding to whole LSB's and will occur as an uncorrectable uncertainty even in ADC's with perfect absolute accuracy. With reference to the drawing shown below, if the digital word is known, the analog input that generated it can only be established with a $\pm 1 / 2$ LSB uncertainty. In the measurement of ADC's, Quantization Error can be eliminated by monitoring transition points.


QUANTIZING ERROR

POWER SUPPLY SENSITIVITY: Most converter specifications are defined at the nominal power supply voltages. Depatures from these specifications will occur at other supply voltages and are usually specified as a worst case degradation per percent change in the power supply voltage. Normally quoted are:

Sensitivity of scale factor to power supply variation
Sensitivity of offset to power supply variation NOTE: Differential Linearity is normally not significantly affected by variations in power supply voltage.

STABILITY: Variations in converter performance due to the passage of time. Converters designed for superior time stability are built with aged components including wirewound resistors. Philbrick recommends product burn-in and temperature cycling for applications requiring the ultimate in stability.

ANALOG NONLINEARITY (MDAC ONLY): The percentage deviation from the best straight line for the analog input to analog output transfer function.

FEEDTHROUGH (MDAC ONLY): The amount of analog output for various input frequencies with the digital word programmed for zero output.

SETTLING TIME - DAC: Settling time for a DAC is the total time necessary for the DAC to complete a full-scale step (including switching, slewing, and small-signal settling) to within a defined error band at the output (normally $\pm 1 / 2$ LSB).
NOTE: Current output DAC's often settle very fast only with a low impedance load. Therefore, the specified settling time may not be attainable in many real system applications, without special circuitry.


DAC DELAY: Deglitched DAC's have a built-in time delay (often variable by external control). This parameter defines the time delay between the strobe leading edge and initiation of the output voltage change, and does not include settling of the output.


DELAY TIME IN DEGLITCHED DAC's

SLEW RATE: The maximum rate at which a DAC output voltage can change in response to a full-scale-output command. Slew rate is only a guide to speed. In most applications, the important specification is the settling time, which is speed to rated accuracy.

CONVERSION TIME: Time required to reach the computed output by an ADC. In successive-approximation converters the conversion time is independent of input amplitude (ranging from $1 \mu \mathrm{Sec}$ to $200 \mu \mathrm{Sec}$ ). In integrating converters the conversion time is somewhat proportional to the input amplitude, varying about 50\% from zero to full scale (ranging from 1 ms to desired noise-eliminating, integrating period). Conversion time for a tracking converter is very fast for small signals ( 100 ns per LSB step change, for example), but will be much longer for large signal charges.

DAC - MAXIMUM WORD RATE: This parameter, (which has many names, e.g. throughput rate, etc.) defines the maximum rate at which a DAC may be commanded to make 1 LSB steps. The Word Rate is necessary to understand the DAC's limitations when driving it from a counter to generate analog ramps.

ADC UPDATE RATE: This is the maximum cyclical rate at which the ADC may make repetitive conversions. NOTE: This is not necessarily equal to the reciprocal of the conversion time, as many converters require time to reset before initiation of the next conversion. Also, in buffered ADC's there must be a time allowance for input settling. The digital output is normally held for at least 1 clock pulse after conversion.

SETTLING TIME - ADC: Settling time for an ADC is the time required after a full scale input change before a conversion may be initiated.
NOTE: Amplified-input ADC's will be slower in this regard because of settling of the input amplifier.

GLITCH: A glitch or transient spike occurs in all DAC's when it changes from one level to another. The glitch is caused by the skewing of analog switches (switches turning on faster than off, or vice versa) and is most pronounced for small changes around the MSB.

## NOTES ON GLITCHES

1.) Glitches in standard DAC's, when measured with infinite bandwidth, may display amplitude peak $=$ Full Scale/2. The pulse width of the glitch will depend upon the skew of the input data as well as the DAC's design. The true measure of the glitch is not its amplitude, but its area (integral) in volt-seconds which is normally unaffected by the bandwidth of the system. The glitch peak amplitude amy be reduced arbitrarily by filtering of the DAC output.
2.) The glitch is often produced when a DAC is fed highskew words.
3.) A well-designed standard DAC with F.S. $=10$ volts when driven from TTL registers can be expected to have a major transition glitch of less than $200 \times 10^{-9}$ volt-seconds.
4.) Deglitched DAC's often have two glitch specifications: a.) The area magnitude of the repetitive glitch, i.e. the glitch that occurs for every transition. This
can often be treated as an offset voltage.
b.) The maximum change in glitch area magnitude as a function of changes in the digital word. This must be considered as equivalent to a dynamic linearity error and when generating a ramp, may not be discernable from a differential nonlinearity error.

timing diagram of deglitched dac

TEMPERATURE PERFORMANCE: In addition to the performance at $+25^{\circ} \mathrm{C}$ specified for a converter, there usually are quoted certain temperature coefficients which define the expected performance degradation per degree departure from the specified temperature. Those most commonly quoted per:
1.) SCALE-FACTOR TEMPERATURE COEFFICIENT: The slope deviation caused by bit weighting resistor ratios, terminating resistor and reference circuitry not tracking perfectly with temperature. The total scale factor change is specified in $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ of reading.
2.) OFFSET TEMPERATURE COEFFICIENT: The overall converter drift with temperature. Caused by switch leakages, output amplifier offset T.C. (voltage DAC's), and buffer amplifier and comparator T.C. (ADC's). Bipolar Offset Temperature Coefficient, for offset binary, is affected mainly by the tracking of the offsetting resistor to the MSB with temperature. Offset Temperature Coefficient is expressed in $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ of full scale.
3.) LINEARITY TEMPERATURE COEFFICIENT
4.) DIFFERENTIAL NONLINEARITY TEMPERATURE COEFFICIENT: Describes the tracking of the bit weights to each other. A converter may have acceptable differential nonlinearity at $25^{\circ} \mathrm{C}$, but at some other temperature it may be greater than 1 LSB, causing the converter to be non-monotonic.

STATIC ERROR ANALYSIS: In any given application the various sources of error must be properly accounted to determine expected system performance. This analysis must be tailored to the specific application. In many applications, for example, differential linearity is important while overall linearity is less important. Other applications are very forgiving of offset and/or scale factor errors.

In the more extreme cases where full absolute accuracy of the transfer function is required, all sources of error must be added for the worst-case condition to be established.

Example: 12-Bit D to A Converter
Assume Scale Factor error and Offset errors are trimmed to zero at $25^{\circ} \mathrm{C}, \Delta \mathrm{T}=50^{\circ} \mathrm{C}, \Delta \mathrm{Vcc}= \pm 1 \%$ Nonlinearity $\pm 0.5$ LSB
Noise

$$
\begin{aligned}
& \frac{ \pm 0.1 \text { LSB }}{ \pm 0.6 \text { LSB }}=1 / 2^{12} \times 0.6= \pm 0.000146 \\
& \text { of F.S. }
\end{aligned}
$$

Scale Factor $\pm 10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}=0.00001$ of value $/{ }^{\circ} \mathrm{C}$.
For $50^{\circ} \mathrm{C}= \pm 0.0005$ of value.
Offset $\pm 5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}= \pm 0.000005$ of F.S. $/{ }^{\circ} \mathrm{C}$. For $50^{\circ} \mathrm{C}= \pm 0.00025$ of $\mathrm{F} . \mathrm{S}$.
Power Supply Sensitivity $\pm 0.002 \% / \% \Delta$ Power Supply. For $\pm 1 \%= \pm 0.00002$ of value.
Max. Total Error $=( \pm 0.000146 \pm 0.0005 \pm 0.00025$
$\pm 0.00002) \times$ F.S. $=(0.000916 \times$ F.S. $)$
(for all conditions at full scale)



ABSOLUTE WORST CASE ERROR BAND FOR A/D CONVERTER - 12 BITS (Gain T.C. $\pm 10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ \& OFFSET T.C. $= \pm 5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ )

ANALYSIS OF DIFFERENTIAL NONLINEARITY VS. TEMPERATURE: The preceding analyses have shown the absolute worst-case errors vs. temperature and power supply, but tell nothing about the differential nonlinearity of the converter. For example, over what temperature range will the converter be monotonic?
Since monotonicity requires differential nonlinearity $\leqslant 1$ LSB, a converter with an initial differential nonlinearity of $\pm 1 / 2 \mathrm{LSB}$ at $25^{\circ} \mathrm{C}$ must have a T.C. $\leqslant 1 / 2 \mathrm{LSB} / \Delta \mathrm{T}$ to maintain monotonicity. Thus, in a 12 -bit converter (where $1 / 2 \mathrm{LSB}=122 \mathrm{ppm}$ of F.S.), monotonicity over a $\pm 50^{\circ} \mathrm{C}$ variation in the worst case requires a differential nonlinearity
T.C. $=\frac{122 \mathrm{ppm}}{50^{\circ} \mathrm{C}}=2.44 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ of F.S., max.

## SAMPLE-HOLD PARAMETER DEFINITIONS

The definitions which Philbrick applies to the key parameters of the 4853 are listed below. To minimize confusion, these definitions are essentially identical to those currently used by other large manufacturers of sample-hold amplifiers.

ACQUISITION TIME: The length of time between the Sample command and the moment the output is tracked to within the specified accuracy.

APERTURE TIME: The apparent time elapsed between the Hold command and the effective opening of the Hold switch. Sometimes referred to as "Turn-off Time".

IMPORTANT NOTE: Some manufacturers use the term aperture time when they are actually referring to aperture uncertainty time. As seen below, these are two completely different specifications.

APERTURE UNCERTAINTY TIME: The tolerance of the delay between a hold command and the actual opening of the hold switch. The variation of the aperture time.

BANDWIDTH: The frequency range over which the unit will operate within the rated accuracy. Although frequencies somewhat higher than this can be applied, the distortion and phase shift encountered may render inaccurate results.

DECAY RATE: The drift encountered when in the Hold mode.

FEEDTHROUGH: The effect of the input signal on the output when the amplifier is in the Hold mode. Usually a function of input signal level and frequency.

GAIN ERROR: The variation from nominal gain caused by component tolerances within the sample-hold amplifier.

GAIN T.C.: The effect that changes in ambient temperature have on the initial gain.

SWITCHING TRANSIENT: Voltage spikes generated when switching to Hold or Sample mode.

HOLD JUMP VOLTAGE: The output voltage step encountered when switching into the Hold mode, caused by a charge transferred to the holding circuit from the switch circuitry.

HOLD OFFSET VOLTAGE: The error voltage encountered when in Hold. This is a dc level that can have either a positive or negative value. It is composed of the Hold Jump Voltage and the Sample Offset Voltage.

SAMPLE OFFSET VOLTAGE: An error voltage encountered in the Sample mode which is due basically to the offset voltage of the internal op-amp. This dc level can have either a negative or a positive value and is one of the components of the Hold Offset Voltage.

APPLYING DATA CONVERTERS: The following pages present the specifications for our data conversion products. The selection of the best converter for the job can be simplified by using the following outline as a guide: D/A Converters Applications Notes
Current Output Models Why use one?
1.) For speed - They can be very fast with a low impedance load. In many cases a high speed operational amplifier is used on the output to achieve faster settling times for a desired voltage output. The ability to select the output amplifier permits circuit "tailoring" for economy and performance.
2.) For voltage scaling - By having a selectable gain operational amplifier on the output you can select the exact scale factor for the application. This method of adjusting the scale factor is far superior to that of varying the reference for a multiplying $D / A$, in terms of linearity.
3.) Driving a terminated line - Line losses will not affect output voltage
4.) Driving a comparator in A/D converters.
5.) Driving an active nonlinear network. Often devices such as logarithmic elements require a current input for maximum performance.
6.) For a power output - A current $D / A$ can be fed directly into a current-to-voltage converter. Using a voltage DAC would put the errors of two amplifiers (and the additional cost) into the system.
7.) For signal multiplexing - Current switching is much faster and accurate than voltage switching.
8.) For driving an analog integrator - For applications such as a digitally controlled timer, a current output D/A interfaces directly with an integrator.

## MULTIPLYING D/A's - IMPORTANT APPLICATIONS

1.) Display Systems
2.) Polar to Cartesian Coordinate Conversion
3.) Square law D/A or $A / D$ conversion
4.) Precision low level multiplier
5.) Circuit linearity correction (Pincushion correction)
6.) Ratio taking $A / D$
7.) Digital-to-Analog converter

## TYPES OF A/D CONVERTERS

SUCCESSIVE APPROXIMATION (S.A.) CONVERTERS FEATURES:
A.) Very fast conversion per bit - even for purely random inputs.
B.) High resolution if desired
C.) Serial output and parallel output
D.) Overall Linearity is good
E.) Answer not dependent upon clock rate

## CONSIDERATIONS:

A.) Signal must not change during the conversion time. Therefore, for many applications the S.A. converter must be preceded by sample and hold. Will not provide average over conversion period.
B.) Differential linearity only fair.

## APPLICATION:

Successive approximation ADC's are most useful for data acquisition systems in conjunction with a multiplexer and high speed sample/hold amplifier. Excellent choice wherever high speed and accuracy are primary considerations.

## INTEGRATING A/D CONVERTER

## FEATURES:

A.) Excellent differential linearity
B.) No sample and hold required for most applications as output will be the average of the input during conversion period.
C.) Modest cost due to internal simplicity.
D.) By using an additional remote counter, single wire data transmission can be obtained.
E.) Answer independent of clock rate and capacitor value in two-slope unit.
F.) Good noise rejection.

CONSIDERATIONS:
A.) This conversion technique is generally slow.
B.) No true serial output is available.
C.) Unipolar only.

## APPLICATION:

The integrating ADC is highly recommended for most applications where high speed is not a requirement. Applications such as digital voltmeters and digital weighing systems take advantage of the noise rejection and differential linearity features of integrating-type ADC's.

## TRACKING CONVERTER

## FEATURES:

A.) No sample and hold required.
B.) Output answer always valid.
C.) Equivalent update rate of 1 clock pulse for continuous signals.
CONSIDERATIONS:
A.) Quantization error $\pm 1$ LSB due to loop hysteresis.
B.) Long conversion time for large signal changes. (Typically 100 to $200 \mu \mathrm{Sec}$ ).
C.) No serial output.

APPLICATION:
Tracking ADC's provide very fast conversion at low cost for applications such as process or servo control systems where the input signal is continuous and one converter can be used per signal input. Other applications include time expansion, transducer, and audio digitizing, and infinite track/hold amplifiers.

| ATO D <br> SPECIFICATIONS | ANALOG TO DIGITAL CONVERTER COMPARISON |  |  |
| :---: | :---: | :---: | :---: |
|  | A TO D TYPES |  |  |
|  | INTEGRATING | TRACKING | SUCCESSIVE <br> APPROXIMATION |
| RESOLUTION \& ACCURACY | Medium to High 8 to 16 Bits | Low to Medium 6 to 10 Bits | Medium to High 8 to 16 Bits |
| LINEARITY | $\begin{aligned} & \pm 1 / 2 \text { LSB to } \\ & \pm 1 \text { Count } \end{aligned}$ | $\pm 1 / 2$ LSB <br> or better | $\pm 1 / 2$ LSB |
| CONVERSION TIME | .5 to 10 mSec SLOW | 6 to $200 \mu$ Sec but will change an LSB in $0.1 \mu \mathrm{Sec}$. Very Fast per LSB | $1 \text { to } 200 \mu \mathrm{Sec}$ <br> Medium to F Fast |
| cost | \$50 to \$200 | \$50 to \$200 | \$50 to \$1,000 |
| OUTPUT | Parallel but count available for Serial | Parallel | Parallel \& Serial |
| ADVANTAGES \& DISADVANTAGES | Best Differential Linearity Least cost/Bit for many Bits High noise rejection SLOW, UNIPOLAR | Follows Input <br> Min. cost $/ \mu$ Sec <br> for one input <br> No latches required <br> No serial output | Serial out standard versatile good cost/speed |
| TYPICAL <br> APPLICATIONS | DVM's <br> Weighing systems | Digitize voice \& $\infty$ time sample \& hold. Time expansion | Data Acquisition. General usage. |
| PHILBRICK MODELS | $\begin{aligned} & 4109,4109 / 10, \\ & 4111,4111 / 10 \end{aligned}$ | 4110 | 4103, 4104, 4105, 4106, 4107, 4108, 4112, 4113, 4114 |

## Digital/Analog Converters

|  | Model | Resolution | Input Code Options ( $\mathrm{T}^{2} \mathrm{~L} / \mathrm{DTL}$ Compatible) | Output Options | Output Impedance (Unipolar/Bipolar) | Settling Time to \% of F.S. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General <br> Purpose <br> Economy | 4020 | 8 -bits | BIN; OBIN | 0 to $+2 \mathrm{~mA} ;-1$ to +1 mA | $8 \mathrm{k} \Omega / 3.5 \mathrm{k} \Omega$ | 300 ns to 0.05\% |
|  | 4021 |  |  | 0 to $-10 \mathrm{~V} ;+5$ to -5 V | $<0.3 \Omega$ | $25 \mu$ s to 0.05\% |
|  | 4022 | 10-bits | BIN; OBIN | 0 to $+2 \mathrm{~mA} ;-1$ to +1 mA | $8 \mathrm{k} \Omega / 3.5 \mathrm{k} \Omega$ | 300 ns to 0.05\% |
|  | 4023 |  |  | 0 to $-10 \mathrm{~V} ;+5$ to -5 V | $<0.3 \Omega$ | 25 ns to 0.05\% |
|  | 4024 | 12-bits | BIN; OBIN | 0 to $+2 \mathrm{~mA} ;-1$ to +1 mA | $8 \mathrm{k} \Omega / 3.5 \mathrm{k} \Omega$ | 300 ns to 0.01\% |
|  | 4025 |  |  | 0 to $-10 \mathrm{~V} ;+5$ to -5 V | $<0.3 \Omega$ | $5 \mu$ s to 0.01\% |
|  | 4026 | 12-bits | BCD | 0 to +1.25 mA | $5 \mathrm{k} \Omega$ | 300 ns to 0.01\% |
|  | 4027 |  |  | 0 to -10 V | $<0.3 \Omega$ | $5 \mu$ s to 0.01\% |
| General <br> Purpose <br> High <br> Performance | 4010 | 10-bits | BIN; OBIN | 0 to $+2 \mathrm{~mA} ;-1$ to +1 mA | $8 \mathrm{k} \Omega / 3.5 \mathrm{k} \Omega$ | 300 ns to 0.01\% |
|  | 4011 |  | OBIN | +10 to -10 V | $<0.3 \Omega$ | $5 \mu$ s to 0.01\% |
|  | 4004 | 12-bits | BIN; OBIN | 0 to $+2 \mathrm{~mA} ;-1$ to +1 mA | $8 \mathrm{k} \Omega / 3.5 \mathrm{k} \Omega$ | 300 ns to $0.01 \%$ |
|  | 4005 |  | OBIN | +10 to -10 V | $<0.3 \Omega$ | $5 \mu$ s to 0.01\% |
|  | 4008 | 12-bits | BCD | 0 to +1.25 mA | $5 \mathrm{k} \Omega$ | 300 ns to $0.01 \%$ |
|  | 4009 |  |  | 0 to -10 V | $<0.3 \Omega$ | $5 \mu$ s to 0.01\% |
| Ultra Fast | 4014 | 12-bits | BIN; OBIN | 0 to $+16 \mathrm{~mA} ;-8$ to +8 mA | $500 \mathrm{k} \Omega \mathrm{min}$. | 100 ns to $0.01 \%$ |
|  | 4016 | 13-bits |  |  |  |  |
| MIL-Grade Microcircuits | 4050 | 8 -bits | BIN; OBIN | 0 to $+3.2 \mathrm{~mA} ;-1.6$ to +1.6 mA | $>3 \mathrm{k} \Omega$ | $0.1 \mu$ s to 0.05\% |
|  | 4051 |  |  | 0 to $-10 \mathrm{~V} ;+5$ to -5 V (11) | $>0.3 \Omega$ | $1 \mu$ s to 0.05\% |
|  | 4052 | 10-bits | BIN; OBIN | 0 to $+3.2 \mathrm{~mA} ;+1.6$ to -1.6 mA | $>3 \mathrm{k} \Omega$ | $0.2 \mu$ s to 0.01\% |
|  | 4053 |  |  | 0 to $-10 \mathrm{~V} ;+5$ to -5 V (1) | $>0.3 \Omega$ | $1 \mu$ s to 0.01\% |
|  | 4054 | 12-bits | BIN; OBIN | 0 to $+3.2 \mathrm{~mA} ;-1.6$ to +1.6 mA | $>3 \mathrm{k} \Omega$ | $0.4 \mu$ s to 0.01\% |
|  | 4055 |  |  | 0 to $-10 \mathrm{~V} ;+5$ to -5 V (11) | $>0.3 \Omega$ | 1 , s to $0.01 \%$ |


|  | Model | Resolution | Input Code ( $\mathrm{T}^{2}$ L/DTL Compatible) | Output | Output Impedance | Noise (RMS) | Glitches (peak) max. | Overshoot max. | Settling Time/ 10 V Step | Slew Rate |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4002 | $\begin{gathered} 14 \text {-bits } \\ \text { (incl. sign) } \end{gathered}$ | Mag \& Sign BIN | $\pm 10 \mathrm{~V}$ | $0.1 \Omega$ | 0.1 mV | $\pm 5 \mathrm{mV}$ | $\begin{gathered} \pm 5 \mathrm{mV} \\ \text { peak } \end{gathered}$ | $20 \mu \mathrm{Sec}$ (6) | $1.8 \mathrm{~V} / \mu \mathrm{Sec}$ |
| Deglitched | 4015 | 12 -bits | OBIN; 2 SC | $\pm 10 \mathrm{~V}$ | $0.1 \Omega$ | 0.5 mV | $\pm 20 \mathrm{mV}$ | $\begin{gathered} 25 \% \text { for } \\ \leqslant 1 \mathrm{~V} \text { Step } \\ \hline \end{gathered}$ | $\begin{gathered} 5 \mu \mathrm{~s} \text { (2) } \\ \text { to } 0.01 \% \end{gathered}$ | $8 \mathrm{~V} / \mu \mathrm{Sec}$ |


|  | Model | Resolution | Input Code ( $\mathbf{T}^{2}$ L/DTL Compatible) | Analog Reference Input | Input <br> Impedance $\min$. | F.S. <br> Output max. | F.S. Gain | Outpu Impedan | $\begin{array}{r} \text { Sett } \\ \text { Digital } \end{array}$ | Time Analog |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4028 | 8 -bits | BIN | $\pm 10 \mathrm{~V}$ | $3 \mathrm{k} \Omega$ | $\pm 10 \mathrm{~V}$ | (-255/256) | $\Uparrow 1 \Omega$ | $5 \mu \mathrm{Sec}$ | $5 \mu \mathrm{Sec}$ |
| Multiplying | 4029 | 10 -bits |  |  |  |  |  |  |  |  |

All specifications are typical at $25^{\circ} \mathrm{C}$ nominal power supply unless otherwise indicated.

1. ABBREVIATIONS

BIN - Binary
OBIN - Offset Binary
BCD - Binary Coded Decimal
2SC - Two's Complement
2. Differential Linearity
3. Full Scale T.C. using internal feedback resistor.
4. 1 TTL Load equals -1.6 mA max. at $\mathrm{V}_{\mathrm{IN}}=+0.4 \mathrm{~V}$
(Lo) and $40 \mu \mathrm{~A}$ max. at 2.4 ( Hi ).
5. All control inputs, outputs, and data output lines are compatible with standard DTL/TTL levels. Logic state switch ' 0 ' is $<+0.8 \mathrm{~V}$; logic state switch ' 1 ' is $>+2.0 \mathrm{~V}$.
6. Operating temperature range for all models, except model 4002 and the MIL-Grade Microcircuits, is $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ with a storage temperature range of $-55^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$. Operating temperature range for model 4002 is $+15^{\circ} \mathrm{C}$ to $+45^{\circ} \mathrm{C}$.
7. Operating temperature range for the MIL-Grade Microcircuits is $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ with a storage temperature range of $-65^{\circ} \mathrm{C}$ to $+155^{\circ} \mathrm{C}$. Industrial temperature versions are available. Consult factory for details.
8. To 1 LSB of final value, maximum. For a 1 LSB step settling tıme is $2 \mu \mathrm{Sec}$.
9. Mating connector supplied: Cinch 250-22-30-170
10. Settling time for a 100 mV step is 200 nSec to $\pm 2 \mathrm{mV}$ of final value.
11. Also, +10 V to -10 V ; +2.5 V to -2.5 V available.

| Zero Offset, max. (Unipolar/Bipolar) | Nonlinearity @ $25^{\circ} \mathrm{C}$ max. | Gain TC ppm $/{ }^{\circ} \mathrm{C}$ max. | Stability <br> Zero TC <br> $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ <br> max. | PSRR $\% / \% \Delta \mathbf{V}_{\mathbf{s}}$ max. | Power Requirements | Mechanical (Package \& Socket) See pages 64-65 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $<50 \mathrm{nA} / \pm 1 / 2 \mathrm{LSB}$ | $\pm 1 / 2$ LSB | $\pm 40$ | $\pm 4$ | $\pm 0.05$ | $\pm 15 \mathrm{~V}$ @ 15 mA |  |  |
| $\pm 1 / 2$ LSB |  |  | $\pm 20$ |  | $\pm 15 \mathrm{~V} @ 20 \mathrm{~mA}$ | (6069) |  |
| $<50 \mathrm{nA} / \pm 1 / 2 \mathrm{LSB}$ | $\pm 1 / 2$ LSB | $\pm 40$ |  | $\pm 0.05$ | $\pm 15 \mathrm{~V}$ @ 15 mA |  |  |
| $\pm 1 / 2$ LSB |  |  | $\pm 20$ |  | $\pm 15 \mathrm{~V} @ 20 \mathrm{~mA}$ | (6069) |  |
| $<50 \mathrm{nA} / \pm 1 / 2 \mathrm{LSB}$ | LSB | +30 |  | +0.05 | $\pm 15 \mathrm{~V} @ 15 \mathrm{~mA}$ | E6 |  |
| $\pm 1 / 2$ LSB |  |  | $\pm 20$ |  | $\pm 15 \mathrm{~V} @ 25 \mathrm{~mA}$ | (6069) |  |
| $<50 \mathrm{nA}$ | LSB | $\pm 30$ |  | $\pm 0.05$ | $\pm 15 \mathrm{~V} @ 15 \mathrm{~mA}$ | E6 |  |
| $\pm 1 / 2$ LSB |  |  | $\pm 20$ |  | $\pm 15 \mathrm{~V} @ 25 \mathrm{~mA}$ | (6069) |  |
| $<50 \mathrm{nA} @ 70^{\circ} \mathrm{C}$ | +1/2 LSB | +20 |  | +0.002 | $\pm 15 \mathrm{~V} @ 15 \mathrm{~mA}$ | E6 |  |
| $\pm 1 / 2$ LSB | -1/2 LSB |  | $\pm 20$ |  | $\pm 15 \mathrm{~V}$ @ 25 mA | (6069) |  |
| $<50 \mathrm{nA} @ 70^{\circ} \mathrm{C}$ | $\pm 1 / 2$ LSB | $\pm 20$ |  | $\pm 0.002$ | $\pm 15 \mathrm{~V}$ @ 20 mA | E6 |  |
| $\pm 1 / 2$ LSB |  |  | $\pm 20$ |  | $\pm 15 \mathrm{~V} @ 25 \mathrm{~mA}$ | (6069) |  |
| $<50 \mathrm{nA} @ 70^{\circ} \mathrm{C}$ | 1/2 LSB | +20 | $\pm 3$ | 0.002 | $\pm 15 \mathrm{~V} @ 20 \mathrm{~mA}$ | E6 |  |
| $\pm 1 / 2$ LSB |  |  | $\pm 20$ | 0.002 | $\pm 15 \mathrm{~V}$ @ 25 mA | (6069) |  |
| $4 \mu \mathrm{~A}$ | $\pm 1 / 2$ LSB (3) | $\pm 20$ | $\pm 10$ | $\pm 0.002$ | $\pm 15 \mathrm{~V}$ @ 150 mA | $\begin{aligned} & \text { E6 } \\ & (6128) \end{aligned}$ |  |
| $\pm 10 \mathrm{ppm}$ of F.S. | +1/4 SB | +45 3 | $\pm 10 / \pm 15$ | 0.002 | $\pm 15 \mathrm{~V}$ @ 15 mA |  |  |
| $\pm 20 \mathrm{mV} / \pm 30 \mathrm{mV}$ | 1/4 LSB |  | $\pm 25 / \pm 30$ | 10.002 | $\pm 15 \mathrm{~V} @ 20 \mathrm{~mA}$ | S5 |  |
| $\pm 10 \mathrm{ppm}$ of F.S. | $\pm 1 / 4$ LSB | $\pm 25$ (3) | $\pm 10 / \pm 15$ | $\pm 0.002$ | $\pm 15 \mathrm{~V}$ @ 15 mA | S5 © |  |
| $\pm 20 \mathrm{mV} / \pm 30 \mathrm{mV}$ |  |  | $\pm 15 / \pm 25$ |  | $\pm 15 \mathrm{~V} @ 20 \mathrm{~mA}$ |  |  |
| $\pm 10 \mathrm{ppm}$ of F.S. | LSB | +15 3 | $\pm 10 / \pm 15$ | +0.002 | $\pm 15 \mathrm{~V} @ 15 \mathrm{~mA}$ | S5 © |  |
| $\pm 20 \mathrm{mV} / \pm 30 \mathrm{mV}$ | -1/4 LSB |  | $\pm 10 / \pm 15$ | -0.002 | $\pm 15 \mathrm{~V}$ @ 20 mA | 5 |  |
| Zero Offset, max. | Nonlinearity @ $25^{\circ} \mathrm{C}$ max. | Gain TC $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max. | Stability <br> Zero TC <br> ppm $/{ }^{\circ} \mathrm{C}$ <br> max. | PSRR $\% / \% \Delta V_{\mathrm{s}}$ max. | Power <br> Requirements | Mechanical (Package \& Socket) See pages 64-65 |  |
| Adj. to 0 V | $\pm 1 / 2$ LSB | $\pm 7$ | $\pm 3$ | $\pm 0.007$ | $\pm 15 \mathrm{~V} @ 35 \mathrm{~mA}$ | E8 (1) |  |
| Adj. to 0 V | $\pm 1 / 2$ LSB | $\pm 20$ | $\pm 10$ | $\pm 0.005$ | $\begin{aligned} & \pm 15 \mathrm{~V} @ 150 \mathrm{~mA} \\ & +5 \mathrm{~V} @ 250 \mathrm{~mA} \end{aligned}$ | E8 ( ) |  |
| Zero Offset, max. | Nonlinearity <br> @ $25^{\circ} \mathrm{C}$ max. | Gain TC $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max. | Stability <br> Zero TC <br> $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ <br> max. | PSRR $\% / \% \Delta \mathbf{V}_{\text {s }}$ max. | Power Requirements | Mechanical <br> (Package <br> \& Socket) <br> See pages 64-65 |  |
| $\pm 2.5 \mathrm{mV}$ | $\pm 1 / 2$ LSB | $\pm 25$ | $\pm 10$ | $\pm 0.002$ | $\pm 15 \mathrm{~V}$ @ 25 mA | $\begin{aligned} & \text { E6 } \\ & (6069) \end{aligned}$ |  |

## Monolithic Quad Current Switch

## FEATURES

- 16 Bit Accuracy
- $0.5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Nonlinearity T.C.
- 30 nSec Settling to Within 0.01\%
- High Current Capability
- 3 nSec Switching Speed
- Operates over +5 to $\pm 15 \mathrm{~V}$
- Low ICBO of 6 pA


## APPLICATIONS

- D/A and A/D Converters
- Meter Drive
- x - y Recorders
- Programmable Voltage Sources
- Micropower D/A Converters
- +5 Volt D/A Converter


REVERSE PINS L \& M TO GET COMPLEMENTARY OUTPUTS. HIGH $=O N$

Philbrick's new monolithic quad current switch Model 3420 is designed for data conversion applications where speed, accuracy, and stability are critical requirements. A switching speed of 3 nSec and a settling time of 30 nSec to $0.01 \%$ permit the design of high speed converters with up to 16 bit accuracy.
A combination of special topographical design and high quality PNP transistors is unique to the Philbrick 3420. This design technique* eliminates "thermal tails" and permits full scale output currents as high as 40 mA or as low as $40 \mu \mathrm{~A}$. Precision matching of the PNP transistors and a superior reference capability ensures exceptionally low T.C. of nonlinearity.
Model 3420 quad switch can be processed to MIL-STD-883 for military or rugged commercial applications and is offered in a 14 pin dual-in-line package.
*Registered U.S. Patent Office

|  | TYPICAL | GUARANTEED |
| :---: | :---: | :---: |
| LOGIC INPUTS ( $\mathbf{T}^{2}$ L) |  |  |
| "0" (Switch Off) . | -- | 0.8 V max, $-40 \mu \mathrm{~A}$ |
| "1" (Switch On) | -- | 2.0 V min,$+0.01 \mu \mathrm{~A}$ |
| OUTPUT CURRENT <br> (For 4.0 mAF F.) |  |  |
| MSB (Bit One) | -- | 2.0 mA |
| BIT 2 | -- | 1.0 mA |
| BIT 3 | -- | 0.5 mA |
| BIT 4 | -- | 0.25 mA |
| OUTPUT CURRENT RANGE |  |  |
| Full Scale | $1 \mu \mathrm{~A}$ to 40 mA | $40 \mu \mathrm{~A}$ to 4.0 mA min. |
| Per Emitter | $0.06 \mu \mathrm{~A}$ to 2.5 mA | $2.5 \mu \mathrm{~A}$ to 0.25 mA min. |
| OUTPUT VOLTAGE |  |  |
| For Rated Accuracy . . | -0.5 to -5 Vdc | 0 to -3.0 Vdc min . |
| Derated | +10 to -20 Vdc | +0.5 to -10 Vdc min. |
| SWITCH CHARACTERISTICS |  |  |
| $\beta$ | 230 | 100 min . |
| $\beta$ Match | $\pm 1 \%$ | -- |
| $V_{\text {BE }}$ Match | $\pm 0.3 \mathrm{mV}$ | -- |
| $\frac{\mathrm{d} \mathrm{~V}_{\mathrm{BE}} \text { Match }}{\mathrm{d} \theta}$ |  | $2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| $\frac{\mathrm{d} a \text { Match }}{\mathrm{d} \theta}$ | $2 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | $10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ max. |
| lebo @ 3 V | 4 pA | 100 pA max. |
| $I_{\text {cbo }}$ @ 5 V | 6 pA | 100 pA max. |
| DYNAMIC CHARACTERISTICS |  |  |
| $f \propto 0.5 \mathrm{~mA}$ | 160 MHz | -- |
| Switching Time Uncertainty | 0.2 nSec | -- |
| Rise Time | 2 nSec | -- |
| Settling Time to 0.1\% | 21 nSec | 100 nSec max. |
| Settling Time to $0.01 \%$ | 30 nSec | 300 nSec max. |
| Nonlinearity | 0.008\% | -- |
| Nonlinearity T.C. | $0.5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | $2 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Trim Range | -- | 2000 ppm max. |

## Microcircuit Digital/Analog Converters



## FEATURES

- 8/10/12-bit Resolution
- $0.8 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Nonlinearity T.C.
- -55 to $+125^{\circ} \mathrm{C}$ Temperature Range
- $2 \mu \mathrm{Sec}$ Settling time to $1 / 2$ LSB of 12 -bits (4055)
- Voltage or Current Output
- Hermetically Sealed
- Complete and Self-Contained
- Feature Philbrick's Proprietary Quad Switch

Philbrick's 4050 Series of microcircuit D/A Converters is designed for applications demanding high performance over a wide temperature range. Complete and self-contained, they include within a small 24-pin double-dual-in-line package (1.39'L $\times 0.80^{\prime \prime} \mathrm{W} \times 0.20^{\prime \prime} \mathrm{H}$ ), a precision reference, resistor network, current switches, and temperature compensation. Voltage output versions also include a high-speed output amplifier.
Models 4050, 4052, and 4054 are current output devices with 8,10 , and 12 -bits resolution, respectively, which feature exceptionally fast settling time ( $0.4 \mu \mathrm{Sec}$ to within $1 / 2$ LSB for 12 -bits) and very low offset and full scale drift with temperature. The current output versions have built-in feedback resistors for use with external amplifiers.
Models 4051, 4053, and 4055 are the corresponding voltage output versions with 8,10 , and 12 -bit resolution, respectively. Incorporated in the design of these DAC's is a special feedback network around the internal operational amplifier which permits the selection of two output voltage ranges in unipolar, and three voltage ranges in bipolar operation. The high speed output amplifier gives a settling time of $2 \mu \mathrm{Sec}$ to within $1 / 2$ LSB for a full scale change.
All 4050 Series DAC's can be operated in the unipolar or bipolar mode. All models incorporate a special reference network and temperature compensation to ensure exceptionally low thermal errors. Hermetic sealing and the exclusive use of high quality components give the 4050 Series excellent reliability in the most demanding applications.
Military versions are also available processed to MIL-STD-883.


## Analog/Digital Converters

|  |  | Model | Resolution | Linearity at $25^{\circ} \mathrm{C}$ max. | Analog Input Options | Output Code Options ( $T^{2}$ L/DTL Compatible) | Input Impedance | Conversion Time, max. (Throughput Time) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tracking |  | 4110 | 8-bits | $\pm 1 / 4$ LSB | $\begin{aligned} & 0 \text { to }-10 \mathrm{~V} \\ & +5 \text { to }-5 \mathrm{~V} \end{aligned}$ | BIN; OBIN | $4 \mathrm{k} \Omega$ | 125 ns/LSB |
| Successive Approximation | General <br> Purpose <br> Economy | 4114 | 8 -bits | $\pm 1 / 2$ LSB | $\begin{aligned} & 0 \text { to }-10 \mathrm{~V} \\ & +5 \text { to }-5 \mathrm{~V} \end{aligned}$ | BIN; OBIN: 2 SC | $4.5 \mathrm{k} \Omega$ | $45 \mu$ Sec |
|  |  | 4113 | 10-bits |  |  |  | $5 \mathrm{k} \Omega$ | $30 \mu \mathrm{Sec}$ |
|  |  | 4112 | 12-bits |  |  |  | $2 \mathrm{k} \Omega$ | $60 \mu \mathrm{Sec}$ |
|  | Low Cost <br> High <br> Performance. | 4105 | 8 -bits | $\pm 1 / 2$ LSB | $\begin{aligned} & 0 \text { to }-10 \mathrm{~V} \\ & +5 \text { to }-5 \mathrm{~V} \end{aligned}$ | BIN: OBIN: 2 SC | $2 \mathrm{k} \Omega$ | $15 \mu \mathrm{Sec}$ |
|  |  | 4104 | 10-bits |  |  |  |  | $20 \mu \mathrm{Sec}$ |
|  |  | 4103 | 12-bits |  |  |  |  | $30 \mu \mathrm{Sec}$ |
|  | High Speed | 4108 | 8 -bits | $\pm 1 / 2$ LSB | $\begin{aligned} & 0 \text { to }-10 \mathrm{~V} \\ & +5 \text { to }-5 \mathrm{~V} \end{aligned}$ | BIN; OBIN: 2 SC | $2 \mathrm{k} \Omega$ | $6 \mu \mathrm{Sec}$ |
|  |  | 4107 | 10-bits |  |  |  |  | $7 \mu \mathrm{Sec}$ |
|  |  | 4106 | 12-bits |  |  |  |  | $10 \mu \mathrm{Sec}$ |
| Integrating |  | 4109 | 12-bits | $\pm 1 / 2$ LSB | 0 to -10 V | BIN | $100 \mathrm{k} \Omega$ | 6 mSec |
|  |  | 410910 |  |  | 0 to +10 V |  |  |  |
|  |  | 4111 | 12-bits | $\pm 112$ LSB | 0 to -10 V | BCD | $100 \mathrm{k} \Omega$ | 2.5 mSec (5) |
|  |  | 411110 |  |  | 0 to +10 V |  |  |  |
| 1. All specifications are typical at $25^{\circ} \mathrm{C}$ nominal power supply, unless otherwise indicated. <br> 3. 1 TTL Load equals -1.6 mA max. at $\mathrm{V}_{\mathrm{IN}}=+0.4 \mathrm{~V}$ ( Lo ) and $40 \mu \mathrm{~A}$ max. at $2.4 \mathrm{~V}(\mathrm{Hi})$. |  |  |  |  |  |  |  |  |
|  | 2. ABBREVIATIONS <br> BIN - Binary <br> OBIN - Offset Binary <br> BCD - Binary Coded Decimal <br> 2SC - Two's Complement <br> CF - Consult Factory |  |  |  | 4. All control inputs, outputs, and data output lines are compatible with standard DTL/TTL levels. Logic state switch ' 0 ' is $<+0.8 \mathrm{~V}$; logic state switch ' 1 ' is $>+2.0 \mathrm{~V}$. |  |  |  |




Timing Diagram for Integrating Models


## Vollage/Frequency Converters

## FEATURES

- Resolution equivalent to more than 13 bits
- Linearity: $\pm 0.008 \%$ (4701) $\pm 0.015 \%$ (4703) $\pm 0.0002 \%$ of F.S. Plus 0.02\% of Signal (4705)
- Stability: $\pm 27 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ (4701)
$\pm 44 \mathrm{ppm} /{ }^{\circ} \mathrm{C}(4703)$
$\pm 47 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ (4705)
- High noise rejection
- DTL/T²L output; 10 -load fan-out


## APPLICATIONS

- Remote control or monitoring
- 2-wire digital transmission
- Electronic testing
- Magnetic tape recording
- Telemetering
- Isolation
- Servo loops
- Arithmetic operations
- Synchronous speed control

TYPICAL CURVES


NOTE: Shaded area indicates
Maximum error band
Voltage-to-Frequency Transfer Characteristic


The Models 4701, 4703, and 4705 Voltage-to-Frequency Converters provide low-cost linear conversion of analog data to a digital pulse train whose repetition rate is proportional to the analog voltage.

The Models 4701, 4703, and 4705 feature advanced monolithic techniques in a modern adaptation of the "Precision Charge Dispenser" circuit principle. The result . . . uncompromised reliability and performance in a tiny, rugged plug-in module. Inherent noise rejection, plus output compatibility with standard or "COSMOS" DTL/²L logic, permits simple and dependable 2-wire digital transmission even through noisy environments to remote areas. Low OEM prices permit economical multiple signals using Models 4701, 4703, or 4705 at each sensor.

## 4701, 4703 Block Diagram*



## ANALOG INPUT

| Full Scale | 0 VDC to +10 VDC (1) |  | 0 VDC to +10 VDC |
| :---: | :---: | :---: | :---: |
| Overrange | +10\% min. |  | +5\% min. |
| Configuration | Single-ended, referred to ground |  | Differential, referred to Ref IN |
| Offset Voltage (Adj. to Zero) | $\pm 3 \mathrm{mV}$ typical; $\pm 10 \mathrm{mV}$ max. |  | $\pm 3 \mathrm{mV}$ typical; $\pm 10 \mathrm{mV}$ max. |
| Impedance | $23 \mathrm{~K} \Omega$ nominal |  | $10 \mathrm{k} \Omega$ nominal |
| Overvoltage Protection | $\pm 15 \mathrm{~V}$ max. input without damage |  | $\pm 150$ max. input without damage |
| FREQUENCY OUTPUT |  |  |  |
| Full Scale Frequency (fout) | 10 Hz to 10 kHz , plus $10 \%$ overrange | 100 Hz to 100 kHz , plus $10 \%$ overrange | 1 Hz to 1 MHz , plus 5\% overrange |
| Linearity | $\pm 0.008 \%$ typical; $\pm 0.05$ max. | $\pm 0.015 \%$ typical; $\pm 0.05 \%$ max. | $\pm 0.001 \%$ typical; $\pm 0.05 \%$ max. |
| Transfer Characteristic | $\mathrm{f}_{\text {out }}=10 \mathrm{kHz} \times(\mathrm{Ein} / 10 \mathrm{~V})$ | $\mathrm{f}_{\text {out }}=100 \mathrm{kHz} \times(\operatorname{Ein} / 10 \mathrm{~V})$ | $\mathrm{f}_{\text {out }}=1 \mathrm{MHz} \times(\operatorname{Ein} / 10 \mathrm{~V})$ |
| Full Scale Factor | $9.900 \mathrm{~V} \pm 0.05 \mathrm{~V}$ (trimmable to | $9.900 \mathrm{~V} \pm 0.05 \mathrm{~V}$ (trimmable to 10.000 V for 100.00 kHz ) | $9.900 \mathrm{~V} \pm 0.05 \mathrm{~V}$ (trimmable to 10.000 V for 1 MHz ) |
| Waveform | Train of DTL/T ${ }^{2} \mathrm{~L}$ - compatible | Train of DTL/T ${ }^{2} \mathrm{~L}$ - compatible | Train of DTL/T ${ }^{2} \mathrm{~L}$ - compatible |
| Output Levels | Pulses, $30 \mu \mathrm{Sec}$ wide | Pulses, $3 \mu \mathrm{Sec}$ wide | Pulses, $0.3 \mu \mathrm{Sec}$ wide |
| "1" (HIGH) | $\begin{aligned} & +5 \mathrm{~V} \pm 0.5 \mathrm{~V} \text { (no load); }+2.4 \mathrm{~V} \mathrm{~min} . \\ & (+0.4 \mathrm{~mA} \text { load }) \end{aligned}$ | $\begin{aligned} & +5 \mathrm{~V} \pm 0.5 \mathrm{~V} \text { (no load); }+2.4 \mathrm{~V} \text { min } \\ & (+0.4 \mathrm{~mA} \text { load) } \end{aligned}$ | $\begin{aligned} & +5 \mathrm{~V} \pm 0.5 \mathrm{~V} \text { (no load); }+2.4 \mathrm{~V} \text { min. } \\ & \text { ( }+0.4 \mathrm{~mA} \text { load) } \end{aligned}$ |
| "0' (LOW) | $+0.10 \pm 0.10 \mathrm{~V} @-16 \mathrm{~mA}$ sink current | $+0.10 \pm 0.10 \mathrm{~V} @-16 \mathrm{~mA}$ sink current | $+0.20 \pm 0.20 \mathrm{~V} @-16 \mathrm{~mA}$ sink current |
| Output Impedance (In High) | $3 \mathrm{k} \Omega$ | $1 \mathrm{k} \Omega$ | $680 \Omega$ |
| Fan-out | 10 standard $\mathrm{T}^{2} \mathrm{~L}$ loads | 10 standard $\mathrm{T}^{2} \mathrm{~L}$ loads | 10 standard $T^{2}$ L loads |
| Short Circuit Protection | Indefinitely to ground without damage | Indefinitely to around without damage | Indefinitely to ground |
| RESPONSE |  |  |  |
| Settling Time to 0.01\% | 1 to 2 cycles plus $20 \mu \mathrm{Sec}$ | 1 to 2 cycles plus $2 \mu \mathrm{Sec}$ | 1 to 2 cycles plus $10 \mu \mathrm{Sec}$ |
| Overload Recovery | 10 msec | 10 msec | 1 msec |
| Allowable.Capacitive Load | 1000 pF for rated performance | 500 pF for rated performance | 100 pF for rated pérformance |
| STABILITY |  |  |  |
| Full Scale (Span) |  |  |  |
| T.C. (PPM $/{ }^{\circ} \mathrm{C}$ of F.S.) | $\pm 24$ typical; $\pm 100$ max . | $\pm 44$ typical $; \pm 150$ max . | $\pm 47$ typical; $\pm 200$ max. |
| Drift |  |  |  |
| Per Day | $\pm 100$ PPM of F.S. | $\pm 100$ PPM of F.S. max. | $\pm 100$ PPM of F.S. |
| Per Month | $\pm 200$ PPM of F.S. | $\pm 200$ PPM of F.S. max. | $\pm 200$ PPM of F.S. |
| Power Supply Sensitivity | $\pm 500 \mathrm{PPM} / 1 \% \Delta \mathrm{~V}_{\text {cc }}$ max. | $\pm 500 \mathrm{PPM} / 1 \% \Delta \mathrm{~V}_{\text {cc }}$ max. | $\pm 500$ PPM/\% $\Delta_{\text {cc }}$ max. |
| Input Offset |  |  |  |
| T.C. (PPM $/{ }^{\circ} \mathrm{C}$ of F.S.) | $\pm 3$ typical; $\pm 10$ max. | $\pm 3$ typical; $\pm 10$ max. | $\pm 3$ typical. $\pm 5$ max. |
| Drift |  |  |  |
| Per Day | $\pm 10$ PPM of F.S. | $\pm 10$ PPM of F.S. | $\pm 10$ PPM of F.S. |
| Per Month | $\pm 20$ PPM of F.S. | $\pm 20$ PPM of F.S. | $\pm 20$ PPM of F.S. |
| Power Supply Sensitivity | $\pm 100 \mu \mathrm{~V} / \% \Delta \mathrm{~V}_{\text {cc }}$ max. | $\pm 100 \mu \mathrm{~V} / \% \Delta \mathrm{~V}_{\mathrm{cc}} \max .$ | $\pm 100 \mu \mathrm{~V} / \% \Delta \mathrm{~V}_{\text {cc }} \max .$ |
| Warm-up Time | $<1$ minute to $0.01 \%$ | $<1$ minute to 0.02\% | $<5$ minute to 0.02\% |
| POWER | $\pm 15 \mathrm{~V}$ @ $\pm 12 \mathrm{~mA}$ | $\pm 15 \mathrm{~V} @ \pm 18 \mathrm{~mA}$ | $\pm 15 \mathrm{~V} @ \pm 32 \mathrm{~mA}$ |
| ENVIRONMENTAL |  |  |  |
| Temperature Rated Derated Storage |  | $\begin{aligned} & 0^{\circ} \mathrm{C} \text { to }+70{ }^{\circ} \mathrm{C} \\ & -40^{\circ} \mathrm{C} \text { to }+85^{\circ} \mathrm{C} \\ & -55^{\circ} \mathrm{C} \text { to }+125^{\circ} \mathrm{C} \end{aligned}$ |  |

(1) Input voltage of Model 470110 is 0 V to -10 V . Other specifications identical to 4701 . Price $\$ 64.00$ (1-9).

Specifications are typical at $+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{cc}} @ \pm 15 \mathrm{~V}$, unless otherwise indicated.


## Frequency/Vollage Converters



FEATURES

- Excellent Linearity 0.008\%, Typ. (4702) 0.006\%, Typ. (4704)
- Low Cost
- Accepts DTL, TTL, HNIL, COSMOS, Sine, Square or Triangular Wave Inputs
- Adjustable Hysteresis for use with Small Signals
- 20 mA Output Rating

APPLICATIONS

- Magnetic and Optical Pickups
- Phase Locked Loops
- Telemetry Systems
- Frequency Monitors
- Remote Data Transmission
- Tachometers
- Flow Meters
- Broadband FM Discriminators
- Doppler Sonar \& Radar
- Frequency vs. Amplitude X-Y Plot

Model 4702: Nonlinearity vs. Input Frequency (Typical)


Model 4704: Nonlinearity vs. Input Frequency (Typical)


Models 4702 and 4704 Frequency-to-Voltage Converters provide lowcost linear conversion of frequency-coded information to a voltage whose amplitude is proportional to the frequency of the input signal. For maximum versatility the input is compatible with DTL, TTL, COSMOS, and High Noise Immunity Logic. Also, a minimum of external components can be used to adjust the hysteresis and biasing so that low level signals and sine-wave inputs can be accurately converted. If a scale factor change is required, an external resistor can be added to give a full scale output with input signals as low as 1 kHz with only a minor reduction in accuracy.

Models 4702 and 4704 can be used Philbrick Models 4701, 4703, and 4705 Voltage-to-Frequency Converters, to provide exceptionally accurate encoding and decoding of data.


Typical Performance Curve: Output Voltage vs. Input Frequency


Typical at $+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{cc}} @ \pm 15 \mathrm{~V}$, unless otherwise indicated.
4702
4704

## FREQUENCY INPUT

| Full Scale | 0 Hz to 10 kHz | 0 Hz to 100 kHz |
| :---: | :---: | :---: |
| Overrange, min. | +10\% | +10\% |
| Input Levels (1) | $\begin{aligned} & -12 \mathrm{~V} \text { to }+0.8 \mathrm{~V}=\text { Low } \\ & +2.0 \mathrm{~V} \text { to }+12 \mathrm{~V}=\text { High }( \pm 15 \mathrm{~V} \text { Fault (2) }) \end{aligned}$ | $\begin{aligned} & -12 \mathrm{~V} \text { to }+0.8 \mathrm{~V}=\text { Low } \\ & +2.0 \mathrm{~V} \text { to }+12 \mathrm{~V}=\text { High }( \pm 15 \mathrm{~V} \text { Fault (2) }) \end{aligned}$ |
| Loading | $\leqslant 1$ TTL Load (3) | $\leqslant 1$ TTL Load (2) |
| Input Pulse Width, min. | $30 \mu \mathrm{Sec}$ for rated accuracy (3) | $2.5 \mu \mathrm{Sec}$ for rated accuracy (3) |
| Input Impedance | $15 \mathrm{M} \Omega$ \|| 8 pF | $3 \mathrm{k} \Omega \\| 5 \mathrm{pF}$ |
| ANALOG OUTPUT |  |  |
| Full Scale Voltage | $\begin{aligned} & 0 \text { to }+9.9 \mathrm{~V} \pm 0.1 \vee \text { © (4702) } \\ & 0 \text { to }-9.9 \mathrm{~V} \pm 0.1 \vee \text { © (470210) } \end{aligned}$ | 0 to $+9.9 \mathrm{~V}, \pm 0.1 \mathrm{~V}$ (4) |
| Offset, $\mathrm{E}_{\text {Os }}$ | $\pm 10 \mathrm{mV}$ max. @ $\mathrm{f}=0 \mathrm{~Hz}$ | $\pm 10 \mathrm{mV}$ max. @ $\mathrm{f}=0 \mathrm{~Hz}$ |
| Linearity | $\begin{aligned} & \pm 0.008 \% \text { Typ., } \pm 0.03 \% \text { max. } \\ & f_{\text {in }}=1 \mathrm{~Hz} \text { to } 11 \mathrm{kHz} \end{aligned}$ | $\begin{aligned} & \pm 0.006 \% \text { Typ; }, \pm 0.05 \% \text { max. } \\ & \mathrm{f}_{\text {in }}=10 \mathrm{~Hz} \text { to } 110 \mathrm{kHz} \end{aligned}$ |
| Output Impedance, max. | $0.05 \Omega,<0.005 \Omega$ Typ. | $0.1 \Omega, 0.01 \Omega$ Typ. |
| Ripple | $\begin{aligned} & 25 \mathrm{mV} \text { p-p@f=1.0 Hz } \\ & 170 \mathrm{mV} \mathrm{rms} @ f=10 \mathrm{kHz} \end{aligned}$ | $\begin{aligned} & 50 \mathrm{mV} \text { p-p@f}=10 \mathrm{~Hz} \\ & 70 \mathrm{mV} \mathrm{rms} @ \mathrm{f}=100 \mathrm{kHz} \end{aligned}$ |
| Output Current, min. © | $\begin{aligned} & +20 \mathrm{~mA} @ \mathrm{~V}_{\mathrm{O}}=+10 \mathrm{~V},(4702) \\ & -20 \mathrm{~mA} @ \mathrm{~V}_{\mathrm{O}}=-10 \mathrm{~V},(470210) \end{aligned}$ | -5 to $+20 \mathrm{~mA}\left(\mathrm{~V}_{\mathrm{O}}=0\right.$ to $\left.+10 \mathrm{~V}\right)$ |
| RESPONSE |  |  |
| Filter Time Constant, | 0.24 mSec ; can be increased with ext. cap. | 0.02 mSec ; can be increased with ext. cap. |
| STABILITY |  |  |
| $\triangle \mathrm{E}_{\text {Os }}$ vs. Temperature, | $\pm 50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}\left( \pm 5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}\right)$ | $\pm 50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}\left( \pm 5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}\right)$ |
| $\Delta \mathrm{E}_{\mathrm{os}} / \Delta \mathrm{V}_{\mathrm{cc}}$, max. | $\pm 50 \mu \mathrm{~V} / \%$ ( $\pm 5 \mathrm{ppm} / \%$ ) | $\pm 50 \mu \mathrm{~V} / \%$ ( $\pm 5 \mathrm{ppm} / \%$ ) |
| $\Delta \mathrm{E}_{\text {OS }} /$ Time | $30 \mu \mathrm{~V} /$ day, $100 \mu \mathrm{~V} / \mathrm{month}$ | $30 \mu \mathrm{~V} /$ day, $100 \mu \mathrm{~V} / \mathrm{month}$ |
| $\Delta \mathrm{V}_{\mathrm{fs}}$ vs. Temp., max. | $100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ | $150 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| $\Delta \mathrm{V}_{\mathrm{fs}} / \Delta \mathrm{V}_{\mathrm{cc}}$ | $300 \mathrm{ppm} / \%$ | $300 \mathrm{ppm} / \%$ |
| $\Delta \mathbf{V}_{\mathrm{fs} / \text { Time }}$ | $10 \mathrm{ppm} /$ day, $30 \mathrm{ppm} /$ month | $10 \mathrm{ppm} /$ day, $30 \mathrm{ppm} /$ month |
| POWER |  |  |
| Voltage ( $\mathrm{V}_{\mathrm{Cc}}$ ) | $\begin{aligned} & \pm 15 \mathrm{~V}, \pm 5 \% \\ & ( \pm 12 \text { to } \pm 18 \mathrm{~V} \text { with derated specs) } \end{aligned}$ | $\begin{aligned} & \pm 15 \mathrm{~V}, \pm 5 \% \\ & ( \pm 12 \text { to } \pm 18 \mathrm{~V} \text { with derated specs) } \end{aligned}$ |
| Quiescent Current, max. | $\pm 12 \mathrm{~mA}$ (no load), | $\pm 22 \mathrm{~mA}$ (no load), |

## ENVIRONMENT \& RELIABILITY

| Temperature | 0 to $+70^{\circ} \mathrm{C}$ Rated |
| :--- | :--- |
|  | -40 to $+85^{\circ} \mathrm{C}$ Derated |
|  | -55 to $+125^{\circ} \mathrm{C}$ Storage |

MECHANICAL E5

1. Hysteresis: 400 mV p-p. nominal
2. Compatible with TTL and DTL Logic. Compatibility with High Noise Immunity Logic (HNIL) or COSMOS can be achieved with a noise immunity as large as 6 V by the addition of an external resistor.
3. Applies to both normally high dc levels with negativegoing pulse trains, or to normally low dc levels with positive-going pulses. The rise and fall times are not critical.

Model 4702: Output Ripple vs. Frequency

4. At $500 \Omega$ Rated Load. Trimmable to +10.000 V or -10.000 V (470210) with an external $500 \Omega$ rheostat at rated input frequency.
5. Output short circuit proofing: indefinite to ground or to +15 V or to -15 V (470210); 5 seconds max. to -15 V or to $+15 \mathrm{~V}(470210)$.
6. Input duty cycle recommended $25 \%$ to $75 \%$ for 100 kHz , $3 \%$ to $97 \%$ for 10 kHz .


## High Speed Sample Hold Amplifier

## FEATURES

- $\pm 1 \mathrm{nSec}$ Max. Aperture Uncertainty Time
- $1 \mu \mathrm{Sec}$ Acquisition Time to $0.01 \%$, Max.
- 0.005\% Linearity
- 300 ns Settling Time to 0.01\%
- 1 mV Maximum Feedthrough
- 20 kHz Bandwidth



## APPLICATIONS

- Data Acquisition Systems
- A/D Converters
- D/A Converters
- Deglitch Circuits


## DESCRIPTION

Model 4853 is a precision high-speed sample-hold amplifier especially designed for high-resolution data conversion systems. A guaranteed acquisition time of $1 \mu \mathrm{Sec}$ to $0.01 \%$ and other electrical characteristics of exceptional stability and accuracy recommend the 4853 for use with fast 12 -bit D/A and A/D converters. Low feedthrough characteristics permit high throughput multiplexing regardless of input signal amplitude or frequency, thus achieving higher system speed without sacrificing resolution.
Model 4853 achieves high performance by innovative circuit design and exclusive use of high quality components. The switching circuit (a proprietary Philbrick design) minimizes aperture time and aperture time uncertainty. The low uncertainty time ( $\pm 1$ nsec, maximum) ensures a lower holding error for a given input $\mathrm{dv} / \mathrm{dt}$.

The gain of model 4853 is -1.000 ; i.e. the output is a precise inversion of the input.
For exceptionally demanding applications, the 4853 can be externally trimmed for zero offset and gain error. In circuits where speed is not essential (such as Analog-Digital converters with a long conversion time) the decay rate can be reduced by adding an external capacitor.
For optimum reliability the 4853 employs input and output short circuit protection. Internal shielding is incorporated to minimize the effects of electrostatic interference and epozy encapsulation rejects environmental effects for high reliability.


Typical Multiplexer with Sample-Hold
Application

| INPUT |  |
| :---: | :---: |
| Analog: |  |
| Voltage | $\pm 10 \mathrm{~V}$ |
| Current | $\pm 5 \mathrm{~mA}$ |
| Impedance | $2 \mathrm{k} \Omega \\|(20 \mathrm{pF}$ series $2 \mathrm{k} \Omega$ ) |
| Digital: |  |
| Sample | $>+2.0 \mathrm{~V}$ (1 TTL load) |
| Hold | <+0.8 V (1 TTL load) |
| TRANSFER CHARACTERISTICS |  |
| Nonlinearity, max | $\pm 0.005 \%$ |
| Gain (nominal at dc) | -1.000 |
| Gain Error, max | $\pm 0.05 \%$ (1) |
| Gain vs Temperature Range, max | $10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| Sample Voltage Offset, max . . | 3 mV (1) |
| Sample Voltage Offset vs Temp. Range, max | $150 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| Hold Voltage Offset, max | 3 mV (1) (5) |
| Hold Voltage Offset vs Temp. Range, max | $200 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ |
| Hold Jump Voltage | $\pm 1 \mathrm{mV}$ (1) |
| Decay Rate, max | $1 \mu \mathrm{~V} / \mu \operatorname{Sec}$ (2) |
| Feedthrough (in Hold) | 1 mV |
| PSRR (tracking), max <br> (single - ended) | $\begin{aligned} & 0.001 \% / \% \Delta \mathrm{~V}_{\mathrm{s}} \\ & 0.01 \% / \% \Delta \mathrm{~V}_{\mathrm{s}} \end{aligned}$ |
| Long Term Stability (per year) | 0.01\% |
| DYNAMIC CHARACTERISTICS |  |
| Output | $\pm 10 \mathrm{~V} @ \pm 5 \mathrm{~mA}$ |
| Bandwidth (referred to dc gain), max | $\begin{aligned} & 20 \mathrm{kHz} \text { to } \pm 0.02 \% \\ & (80 \mathrm{kHz} \text { to }-0.1 \% \text { typ) } \end{aligned}$ |
| Slew Rate | $30 \mathrm{~V} / \mu \mathrm{sec}$ |
| Aperture Time (ref. to signal input), max | 0 to 10 nsec |
| Aperture Uncertainty Time, max | $\pm 1$ nsec |
| Acquisition Time |  |
| ( 10 V step) to $0.01 \%$ F.S. max | $1 \mu \mathrm{sec}$ |
| (10 V step) to 0.1\% F.S. . | 600 nsec |
| $(20 \mathrm{~V}$ step) to $0.01 \% \mathrm{~F}$. S. max | $1.5 \mu \mathrm{sec}$ |
| (20 V step) to 0.1\% F.S. | $1 \mu \mathrm{sec}$ |
| Sample to Hold Transient | 20 mV |
| Settling Time Switching to Hold |  |
| to 0.01\% F.S., max | 300 nsec |
| to $0.1 \% \mathrm{~F} . \mathrm{S}$. | 100 nsec |
| Phase Shift, max | $0.01{ }^{\circ}$ at 20 kHz |
| POWER REQUIREMENTS |  |
| Voltage | $\pm 15 \mathrm{~V}$, $\pm 2 \%$ |
| Current (quiescent) max | $\pm 30 \mathrm{~mA}$ |
| TEMPERATURE RANGE |  |
| Operating: Rated | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| Storage . . . . | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ |

## Notes:

(1) Trimmable to zero.
(2) May double each $+10^{\circ} \mathrm{C}$, ref. $+25^{\circ} \mathrm{C}$.
(3) Full Scale is considered to be 10 V , therefore $0.01 \%$ is 1 mV .
(4) Warm-up Time for Model 4853 is typically 10 minutes.
(5) Worst case conditions for Sample Voltage Offset and Hold

Jump Voltage will not occur simultaneously.

## The Importance of Feedthrough

The typical data acquisition system consists of an input multiplexer followed by a sample-hold amplifier which buffers an analog-to-digital converter. If the sample-hold has a high feedthrough, a changing input signal will significantly affect the output. The multiplexer, therefore, cannot be switched during the ADC's conversion time without causing intolerable ${ }^{*}$ error, thus limiting data through-put.

The 4853's exceptional feedthrough characteristics are nonlinear and independent of frequency. A clamping network is used to limit the feedthrough to $\pm 1 \mathrm{mV}$ maximum for a 20 volt input step. This permits increased through-put in data acquisition systems.


## NONLINEAR PRODUCTS

Many natural processes are neither linear nor quantitative but behave in continuously smooth, nonlinear ways. To the systems engineer faced with solving nonlinear applications, Teledyne Philbrick offers a wide variety of circuit modules. Armed with a basic knowledge of operational amplifier theory, the engineer can easily understand and apply these nonlinear function modules to extend the mathematical versatility of op amps and provide exponential, transcendental, and high order functions.

Just as the gain is varied in a linear circuit by varying the ratio of the feedback impedance to the input impedance, so does the ratio of impedances for nonlinear circuits, but instead of being a fixed value its varitations, determined by the input amplitude: Also, nonlinear function circuits have basic limitations similar to those of operational amplifiers; dynamic range, bandwidth, conformity, voltage offset, etc.

## WHAT IS A NONLINEAR CIRCUIT?

A circuit is nonlinear when the output is not linearly proportional to its input. Obviously, all digital circuits and amplifiers with unintentional distortion fall in this category; but these are not the products to be discussed here. Rather, we are interested only in those amplifiers having intentional, accurately predetermined, stable distortion. Usually for circuit modules the shape of the distortion can be accurately described by a simple and useful mathematical expression.

The products that we are mainly interested in are logarithmic devices, sine and cosine functions, square law modules, and multiplier/divider modules. Also available are modules whose output can be user-adjusted to virtually any function of the input. These are known as variable function modules.

## VARIOUS CIRCUIT TECHNIQUES

There are two fundamental techniques which are used in generating nonlinear functions, and each technique has its own unique characteristics. Historically, the first method of generating nonlinear functions was the piece-wise, straightline approximation technique using diode-resistor networks which resulted in several advantages and disadvantages. The advantages offered by this technique are as follows:

1. Made fast with varying degrees of "accuracy."
2. Economically manufactured.
3. Used to synthesize almost any function.
4. Usually quite stable versus time and temperature.
5. Generally offers low noise.

The disadvantages include:

1. Narrow input dynamic range.
2. Inputs usually requiring full-scale inputs of at least 10 volts.
3. Output cannot be differentiated (passed through a high pass filter) since the first and greater derivatives are dicontinuous; glitches will appear in the differentiated output.

The second technique used in generating nonlinear functions is the continuous method which uses the nonlinear voltage/current characteristics of semiconductor materials and junctions such as used in log modules and transconductance multiplier/divider modules. The advantages offered by this second technique are as follows:

1. Wide input dynamic range.
2. Usually built compactly.
3. Cost can be very low.
4. Speed is moderate.
5. Output can be differentiated.

The disadvantages include:

1. Elaborate temperature compensation, internal or external, is required.
2. High output noise for certain functions.
3. Choice of desired functions is limited.

The first step in choosing a nonlinear module is to determine which of the two methods of nonlinear generation is most suitable for the application. Of course, some applications require modules with performance beyond the present state-of-the-art. If this is the case, reduced performance or another method should be considered.

## WHAT IS ACCURACY?

Next to cost, the most important consideration for the customer engineer is some figure of merit, usually dubbed "accuracy," which he can use to calculate his overall system error. "Accuracy," however, is a rather nebulous term when applied to intentionally nonlinear operations. The term is primarily suited for defining error of straight-line phenomenon in terms of only three simple parameters: offset, slope, and deviations from straight-line. With linear circuits it is easy to select a reference to which errors can be compared in order to generate an accuracy specification. However, for nonlinear operations, it is necessary to look at the general case from which accuracy is derived, using some simple assumptions.

In the general case, error must be defined in terms of three more complex parameters: offsets, curvature, and deviation from ideal curvature, whereas the curvature is just a straightline for the linear case. Also, in the general case, no assumptions can be made about the proportionality of input and output offsets which would allow the combination of error contributions by simple addition. To more easily understand the error definition, the input and output must be treated separately. It is really meaningless to combine the two errors for an overall accuracy specification because it depends on the amplitude of the input. As a result, it is necessary to calculate accuracy for the various regions or decades of input from the following general transfer function:

$$
\mathrm{E}_{\mathrm{O}}=\mathrm{E}_{\mathrm{O}_{\text {ref }}} \mathrm{F}\left[\frac{\left(\mathrm{l}_{\text {in }} \pm \mathrm{l}_{\mathrm{os}}\right)}{ \pm \mathrm{I}_{\text {ref }}}\right]-\mathrm{E}_{\mathrm{oos}}
$$

For functions with more than one input variable, such as logratio circuits, multipliers, and dividers, each of the inputs must be associated with its own, like-dimensioned (voltage/ current), offset and reference.
The output and its tolerance can be easily calculated under any condition with the above relationship as a foundation, provided the magnitude, tolerance, temperature coefficient, and power supply dependence of both the input and output references and offsets are known. If the deviation from true function conformity is also considered, probable error and worst case errorbands can be calculated over the entire input range in any application. In other words, the most important specifications to the user is a unique combination of those specifications which take into account the user's particular requirements including dynamic range, temperature range, power supply variations, and any other relevant considerations.

## LIMITATIONS WITH FREQUENCY

We have only been looking at the steady-state or lowfrequency operation in determining optimum performance. For high frequency operations, additional considerations are necessary.

For linear systems, the simple parameters of small-signal gain-bandwidth product and output slewing rate are generally sufficient, since the gain is constant, and, therefore, bandwidth is constant. However, in nonlinear circuits, the small-signal gain (or slope) is a function of input level. Therefore, since the gain-bandwidth product tends to remain constant, the small-signal bandwidth will change as a function of input level. Example:


For an amplifier with a 10 MHz gain-bandwidth product at a current level of 1 nA , the maximum operating frequency is approximately equal to 100 Hz .

Similarly, the slewing rate tends to be proportional to small-signal bandwidth. Therefore, slewing rate also changes as a function of input level. Generally, slewing time from one level to another level becomes proportional to the small-signal bandwidth at the final level. In other words, if it takes a certain amount of time in seconds to go from 1 nA to 10 nA then it will take approximately 10 times longer to go from 10 nA to 1 nA . One usually will find the small-signal bandwidths and slewing times are specified at several input levels.

## PARAMETER DEFINITION AND MEASUREMENT GUIDE

SIX PARAMETERS are common to all nonlinear function elements and operators and their significance should be fully appreciated before any attempt is made to evaluate or predict their performance or the performance of a circuit using them.

## - Performance Range

States the values of input signal levels for which the specified input/output relationship will be maintained to the specified accuracy. Several ranges are possible, depending on accessories, the amplifier, and the circuit used.

## - Accuracy

Is stated in terms of conformance with the specified input/output function. It is frequently given in terms of the maximum per-unit or percent error, under "standard" conditions listed in the accuracy specification, and the error expression is usually a fairly simple function of the input (or output) signal level.

## - Temperature Coefficient

Relates the (steady-rate) ambient temperature to the worst-case error (at equilibrium, all other conditions being standard) in the input/output function.

## - Response Error

Relates the dynamic (small signal or transient) performance of the nonlinear element or operator to its dc (steady-state) performance; either by stating the (sinusoidal-wave) frequency rate over which the "standard conditions" performance will be maintained, or by stating a slewing rate, or a settling time.

## - Excitation Dependence

All nonlinear elements and operators require a near perfect signal source. When voltage is the independent variable, it should be supplied by the very low closed loop output impedance of an Operational Amplifier.
When current is the independent variable, it should be provided by an Operational Amplifier programmed as a current pump.

## - Power Supply Dependence

Nonlinear elements and operators that require power supply potentials (such as synthesized function devices) should be used with accurate, well regulated supplies. To ensure optimum performance $0.05 \%$ absolute accuracy is recommended for the supply.

## FEATURES

- Wide Dynamic Range
- Temperature Compensated
- Superior Logarithmic Conformity
- Very Low Cost (Models 4350/4351)

- Log or antilog obtained with built-in Operational Amplifier (Models 4350/4351)
- Adjustable Gain and Reference Current Controls (Models PPL4-N/P)
- Log of Current Ratio (Model 4361)
- Unique Nonlinear Module, Sinh ${ }^{-1}$ Linear through Zero, then Three Decades of AC/DC Logging (Model 4356)
- 40 dB of Speech Compression (Model 4356)


## BASIC CIRCUIT



LOG OF CURRENT (POSITIVE SIGNAL)


WHEREK = SLOPE IN VOLTS/DECADE $i_{\text {in }}=$ INPUT CURRENT $-e_{\text {in }} / R_{\text {in }}$ $I_{\text {ref }}=$ REFERENCE CURRENT $E_{\text {OS }}$ = OUTPUT OFFSET VOLTAGE

Teledyne Philbrick logarithmic amplifiers provide an output proportional to the log or antilog of their input signal. (Model 4361 provides an output proportional to the $\log$ of its input signals only). Each unit is complete with a built-in operational amplifier and a precision antilog element, and requires only operating power plus input and output connections in order to perform its log or antilog computations.
Models 4357/4358 when utilized with two low-bias-current operational amplifiers will produce an accurate, temperature-compensated logarithmic ratio amplifier calibrated to 1 volt per decade input change which responds to 6 decades of input current or 4 decades of input voltage.
Models PPL4-N/P when operated with one low bias current operational amplifier, produces an accurate, temperature-compensated logarithmic amplifier allowing adjustment of reference current and slope (volts per decade input change). Registered U.S. Patent Office.
Model 4350 computes the logarithm of a positive voltage or current or solves for the positive antilog of an input voltage, while the Model 4351 computes the logarithm of a negative voltage or current or solves for the negative antilog of an input voltage. No external amplifiers are required.
Model 4361 is a logarithmic module designed to give an output voltage proportional to the log ratio of its input currents. The inputs require negative current sources in the range of $-10^{-9}$ to $-10^{-3}$ amperes making it ideally suited for phototube ratio applications circuits. This unit is complete with a built-in operational amplifier and precision temper-ature-compensated log-ratio element and has a grounded metal case to shield out unwanted electrostatic noise.
Model 4356 is a temperature-compensated, continuous-function network whose output voltage is proportional to the inverse hyperbolic sine $\left(\sinh ^{-1}\right)$ of the applied input signal. This ac logarithmic amplifier is very useful in applications where a very-wide-dynamic range signal must be recorded or transmitted. By the interconnections on the module, the inverse function can also be generated so that the exact information can be recovered.

| DYNAMIC RANGE |  |  |  |  |
| ---: | :--- | :--- | :--- | :--- |
| Current | 120 dB | 120 dB | 120 dB | 120 dB |
| Voltage | 80 dB | 80 dB | 80 dB | N/A |

ACCURACY
1\% OF READING
(Referred to Input)

| 1 nA to 10 nA | $1 \%$ | $2 \%$ | $1 \%$ | $0.5 \%$ |
| :--- | :--- | :--- | :--- | :--- |
| 10 nA to $100 \mu \mathrm{~A}$ | $1 \%$ | $1 \%$ | $0.5 \%$ | $0.5 \%$ |
| $100 \mu \mathrm{~A}$ to 1 mA | $1 \%$ | $2 \%$ | $1 \%$ | $1 \%$ |

TEMPERATURE
DRIFT

| Scale Factor |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| +10 to $+60^{\circ} \mathrm{C}$ | $\pm 0.04 \% /{ }^{\circ} \mathrm{C}$ | - | - | - |
| -25 to $+85^{\circ} \mathrm{C}$ | - | $\pm 0.04 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.04 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.04 \% /{ }^{\circ} \mathrm{C}$ |
| Offset |  |  |  |  |
| +10 to $+60^{\circ} \mathrm{C}$ | $\pm 0.1 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ | - | - | - |
| -25 to $+85^{\circ} \mathrm{C}$ | - | $\pm 5 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ | $\pm 0.3 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ | $\pm 0.3 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| SLOPE |  |  |  |  |
| Fixed | $1 \mathrm{~V} /$ Decade | - | 1,2,2/3 V/Dec | $1 \mathrm{~V} / \mathrm{Dec}$ |
| Adjustable | Yes | Yes | Yes | Yes |
| RATED OUTPUT |  |  |  |  |
| Current | Depends on Amplifier | Depends on Amplifier | $\pm 10 \mathrm{~mA}$ | $\pm 5 \mathrm{~mA}$ |
| Voltage | Depends on Amplifier | Depends on Amplifier | $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ |
| BANDWIDTH |  |  |  |  |
| 1 nA | 80 Hz | 80 Hz | 80 Hz | 80 Hz |
| $1.0 \mu \mathrm{~A}$ | Depends on Amplifier | Depends on Amplifier | 70 kHz | 70 kHz |
| $10 \mu \mathrm{~A}$ | Depends on Amplifier | Depends on Amplifier | 180 kHz | 180 kHz |
| 1 mA | Depends on Amplifier | Depends on Amplifier | 200 kHz | 200 kHz |
| CASE STYLE | A6 | AS2 | G2 | G1 |
| SOCKET | NSK-20 | US-PP | NSK-20 | NSK-9 |

1. Specifications are typical @ $+25^{\circ} \mathrm{C}$, nominal supply voltage, unless otherwise specified.


Translucent Measuring Circuit Application
An important application using the ratio of log ratio of two inputs is the measurement of the amount of light passing through translucent materials. It is interesting to note that although the intensity of the light source may vary due to temperature or age, the ratio output in decibels does not change because PMT-2 is used as a variable references. Since the material measured may vary from window glass to an opaque metal sheet, the advantage of a logarithimic output is easily recognized.

OUTPUT FUNCTIONS

| $\text { Sinh }^{-1} \quad K_{\sinh }{ }^{-1} \frac{l_{\text {in }}}{2 i_{r}}$ | $\begin{aligned} \mathrm{I}_{\text {in }} & =0 \text { to } \pm 5 \mathrm{~mA} \\ \mathrm{i}_{\mathrm{r}} & =1 \mu \mathrm{~A} \pm 2 \% \end{aligned}$ |
| :---: | :---: |
| $\log _{10} \quad 2.3 \mathrm{Klog} 10 \frac{\mathrm{I}_{\text {in }}}{\mathrm{I}_{r}}$ | $\begin{aligned} & I_{\text {in }}=3 \mu \mathrm{~A} \text { to } \pm 5 \mathrm{~mA} \\ & \mathrm{I}_{\mathrm{r}}=1 \mu \mathrm{~A} \pm 2 \% \end{aligned}$ |
| $(\mathrm{K}=1.000)$ | Adj. with ext. Rf |
| CONFORMITY ( 100 Hz ) |  |
| $\operatorname{Sinh}^{-1}(0.1 \mu \mathrm{~A}$ to $\pm 5 \mathrm{~mA})$ | 0.5 dB |
| Log ( $\pm 3 \mu \mathrm{~A}$ to $\pm 5 \mathrm{~mA}$ ) | 0.5 dB |
| COMPRESSION | 40 dB |
| INPUT |  |
| Voltage | $\pm 10 \mathrm{~V}$ |
| Current | $\pm 5 \mathrm{~mA}$ |
| OUTPUT |  |
| Voltage | $\pm 10 \mathrm{~V}$ |
| Current | $\pm 5 \mathrm{~mA}$ |
| BANDWIDTH |  |
| Large Signal | 10 kHz |
| TEMPERATURE STABILITY |  |
| Offset | $\pm 2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| Scale Factor | $\pm 0.01 \% /{ }^{\circ} \mathrm{C}$ |
| Reference | $\pm 0.1$ \%/ ${ }^{\circ} \mathrm{C}$ |
| TEMPERATURE RANGE | $0^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |
| POWER REQUIREMENT |  |
| Voltage | $\pm 15 \mathrm{~V}$ |
| Current | $\pm 7 \mathrm{~mA}$ |
| CASE STYLE | E1 |
| SOCKET | NSK-14 |

1. Specifications are typical @ $+25^{\circ} \mathrm{C}$, nominal supply voltage, unless otherwise specified.


This module is also useful in applications where a nonsaturat ing amplifier is needed such as in speech communication. Should the ambient noise be much greater than the desired input causing a linear preamplifier to saturate, the nonlinear amplifier will operate to keep the peak levels approximately constant.

## Multiplier/Dividers



## FEATURES

- 0.25\% Accuracy
- 5 MHz Bandwidth
- 4 Quadrant Multiplication


## APPLICATIONS

- Multiplying/Dividing
- Squaring/Square-rooting
- Root-mean-Squaring
- Suppressed Carrier Modulation
- Instantaneous Power Measurement


MODELS 4454, 4455, 4456, and 4457
Philbrick Models 4454, 4455, 4456, and 4457 variable transconductance multiplier/dividers achieve high performance without external amplifiers or trimming networks. Models 4454 and 4455 feature maximum full scale error (untrimmed) of $0.5 \%$ and $0.25 \%$ respectively. Models 4456 and 4457 are high speed units with 5 MHz bandwidth and a maximum untrimmed full scale error of $1 \%$ and $0.5 \%$ respectively. For all models the maximum error is specified for all four quadrants.

In combination with their high initial accuracy these multipliers exhibit exceptionally low drift due to temperature to keep a low total error budget. For the most demanding applications these units can be externally trimmed for feedthrough. In the division mode trimming is optional, but output offset voltage should be trimmed to ensure the widest dynamic range of operation.

The 4 quadrant analog multiplier is an extremely versatile device. The availability of low cost, high performance units has greatly increased the number and type of applications in all areas of industry. Philbrick's years of experience in applying analog technology have given our Applications Department the skills to solve the toughest applications problems. Therefor if you have any questions or need technical assistance, do not hesitate to contact us directly or through your local representative.

## MODELS 4450 and 4452

Model 4450 features a maximum error of $1 \%$ and a 1 MHz bandwidth. Model 4452, Philbrick's lowest cost multiplier features a maximum error of $2 \%$ in four quadrants, ( $1 \%$ in two quadrants) and a built-in division capability.


Specifications are typical at $+25^{\circ} \mathrm{C}$, nominal supply voltage, unless otherwise indicated

## MODEL PPT\&H

## Track-and-HoldOperator



## FEATURES

- High OFF Resistance $-10^{11} \Omega$
- Low ON Resistance - $300 \Omega$
- Fast Aperture Time - < 100 nsec
- Fast Acquisition Time $-<2 \mu \mathrm{sec}$


## DESCRIPTION

The Model PPT \& H Track and Hold Modulator is designed to function with all Teledyne Philbrick Operational Amplifiers and is optimized for use with FET input amplifiers. Performance, especially input current characteristics, will deviate from the specifications depending on the parameters of the amplifier selected. When used with a single operational amplifier, the overall circuit will track an input signal until a logic input is applied that opens the input, holding the output at the same level it had before switching.
SPECIFICATIONS

| INPUT |  |
| :---: | :---: |
| Voltage | $\pm 10 \mathrm{~V}$ |
| Impedance | ON-300 $\Omega$ |
|  | OFF- $10^{11} \Omega$ |
| SWITCHING DELAY GOING |  |
| INTO HOLD | 100 ns Typical |
| SWITCHING DELAY GOING |  |
| OUT OF HOLD | $<2 \mu \mathrm{sec}$ |
| SWITCHING JUMP GOING |  |
| INTO HOLD | $\pm 50 \mathrm{mV}$ max ${ }^{*}$ |
|  | X |
| LOGIC INPUT | $\pm 1 \mathrm{~V}:+1 \mathrm{~V}$ for track |
|  | -1V for hold |
| POWER REQUIREMENT |  |
| Voltage | $\pm 15 \mathrm{~V}$ |
| Current | $\pm 1 \mathrm{~mA}$ |
| CASE STYLE | AS2 |
| SOCKET | US-PP |

MODEL 4352

## Avg-RMS-Vector Operator



## FEATURES

- Calculating the square root of the sum of the squares of two signals
- Finding RMS values of a signal
- Finding average rectified values of a signal
- Plus, minus or AC input signal
- No external circuits required (trim control optional)


## DESCRIPTION

The average-RMS-Vector Operator Model 4352 is a compact, encapsulated unit designed to: find the average value of an input signal, $Y$; find the RMS value of an input signal, $X$; or perform the operation $\sqrt{X^{2}+Y^{2}}$ on the input signals $X$ and $Y$. Averaging and RMS operation is based on instantaneous values of one input signal, with the output appearing as a positive voltage. The operation $\sqrt{\mathrm{X}^{2}+\mathrm{Y}^{2}}$ is based on instantaneous values of two input signals. The output is a positive voltage, and is the instantaneous value of the function. Also by using two Model 4352 units, the operation $\sqrt{X^{2}+Y^{2}+Z^{2}}$ can be obtained. The small size and the multiple functions of which the Model 4352 is capable make it ideally suited for use as a computing element in the laboratory or in manufacturing equipment. Reliable accuracy is provided over a wide range of temperatures and operating conditions.

SPECIFICATIONS

| OUTPUT FUNCTION | RMS | Average Rectified | $\sqrt{X^{2}+Y^{2}}$ |
| :---: | :---: | :---: | :---: |
| INPUT |  |  |  |
| Voltage |  |  |  |
| X | $\pm 10 \mathrm{~V}$ |  | $\pm 10 \mathrm{~V}$ |
| Y |  | $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ |
| Current | 0.75 mA | 1 mA |  |
| OUTPUT |  |  |  |
| Voltage | $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ | $\pm 10 \mathrm{~V}$ |
| Current | $\pm 2 \mathrm{~mA}$ | $\pm 2 \mathrm{~mA}$ | $\pm 2 \mathrm{~mA}$ |
| ACCURACY OF FULL SCALE | $\pm 3 \%$ | $\pm 1 \%$ | $\pm 1 \%$ |
| BANDWIDTH |  |  |  |
| -3 dB . | 20 kHz | 20 kHz | 1 kHz |
| TEMPERATURE STABILITY. |  | $\pm 0.1 \% /{ }^{\circ} \mathrm{C}$ |  |
| TEMPERATURE RANGE . |  | 0 to $+75^{\circ} \mathrm{C}$ |  |
| POWER REQUIREMENTS |  |  |  |
| Voltage |  | $\pm 15 \mathrm{~V}$ |  |
| Current |  | $\pm 30 \mathrm{~mA}$ |  |
| CASE STYLE |  | G1 |  |
| SOCKET | $\cdots \cdot$ | NSK-9 |  |

## MODELS SPFX-N/P

Variable FunctionElements


## FEATURES

- $\pm 0.1 \%$ Accuracy
- Temperature Compensated ( $<100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ )
- Wide Bandwidth
- Output Function Adjustable by User


## DESCRIPTION

The Models SPFX-N and SPFX-P are variable function elements consisting of ten-section temperature compensated, diode-resistor networks having uniformly spaced, fixed breakpoints. The desired function is approximated by eleven straight line segments whose slopes are adjusted by potentiometers accessible on the top of the case. The transition from one segment to the next occurs at one volt intervals of input voltage, from 0.5 V to 9.5 V . When used in the recommended operational amplifier circuits, they will accept an input voltage and generate an output voltage proportional to the desired function. The function generated may be, to a good accuracy, any arbitrary continuous function.
Separate versions of the SPFX are available for positive going (SPFX-P) and negative going (SPFX-N) inputs. One of each may be used in combination for the generation of functions having inputs of both signs. When necessary, closer approximation may be achieved by incorporating additional SPFX units (having the same polarity gender) to obtain finer subdivisions of the curve.

## SPECIFICATIONS

| OUTPUT FUNCTION | User Adjustable |
| :---: | :---: |
| Number of Segments | 11 |
| Breakpoint Spacing | 10 Breakpoints, ea 1V @ 0.5 V |
| Accuracy when operated as square law device @ $25^{\circ} \mathrm{C}$ | $\left\|\delta i / i_{\text {max }}\right\|<0.001$, where $\delta i=(i$ actual $)-(i$ desired $)$ |
| INPUT |  |
| Voltage | 0 V to $-1+10 \mathrm{~V}$ |
| Current | $50 \mu \mathrm{~A}$ max |
| OUTPUT |  |
| Current | 0 mA to $-1+1 \mathrm{~mA}$ |
| BANDWIDTH |  |
| -3 dB Response. | $>500 \mathrm{kHz}$ |
| TEMPERATURE STABILITY. | $< \pm 100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| TEMPERATURE RANGE | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| POWER REQUIREMENTS |  |
| Voltage | $\pm 15 \mathrm{~V}, \pm 0.01 \%$ |
| Current | $\pm 3.5 \mathrm{~mA}$ |
| CASE STYLE | SP |
| SOCKET | MB-SP Supplied |

MODELS 4353/4354

## Square Law Elements



## FEATURES

- $\pm 0.1 \%$ Accuracy
- Low Temperature Coefficient, $<100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
- Wide Bandwidth


## DESCRIPTION

The Models 4353 and 4354 are temperature compensated, straightline approximation, ten-section diode function fitters that have break points adjusted to fit a square law relationship. They are designed to produce, to a good accuracy, an output voltage proportional to thesquare of the input voltage when connected to an appropriate operational amplifier. When used as the input network of an operational amplifier 4354 takes positive inputs and gives a negative output. When used as the feedback element of an operational amplifier to extract square roots, 4354 takes negative inputs and results in a positive output, while 4353 takes negative inputs and results in a negative output. Several applications using these modules include meansquare and RMS computation, odd-value or ab-squaring or rooting, and "quarter square" multiplication.

## SPECIFICATIONS

| OUTPUT FUNCTION | $\mathrm{Y}=+1-\mathrm{X}^{2}$ |
| :---: | :---: |
| Number of Segments | 11 |
| Breakpoint Spacing | 10 Breakpoints, each 1 V @ 0.5 V |
| Accuracy (1) $\begin{array}{r}(4353 \& 4354) \\ (4359 \& 4360)\end{array}$ | $\pm 0.1 \%$ of full scale <br> $\pm 0.25 \%$ of full scale |
| INPUT Voltage Current | $\begin{aligned} & 0 \text { to }-1+10 \mathrm{~V} \\ & \text { Constant }-/+50 \mu \mathrm{~A} \end{aligned}$ |
| OUTPUT | 0 to $-1+0.5 \mathrm{~mA}$ |
| BANDWIDTH |  |
| 1\% Absolute Accuracy (2) | 100 kHz |
| TEMPERATURE STABILITY | Typically $\pm 0.005 \% /{ }^{\circ} \mathrm{C}$ |
| TEMPERATURE RANGE | $-25^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ |
| POWER REQUIREMENT | $\pm 15 \mathrm{~V}, \pm 1.5 \mathrm{~mA}$ |
| CASE STYLE | E5 |
| SOCKET | NSK-20 |

[^0]
## Three Mode Integrator



## FEATURES

- Three Operating Modes, Reset/Integrate/Hold Track/Hold, Electronic Switch
- Command Signals can be of Positive or Negative Polarity
- Uncommitted Comparator Inputs Permit Compatibility to DTL/TTL Digital Logic and Gated Analog Logic
- Internal Bound Circuit Reduces Overdrive Recovery Time
- Accommodates Wide Range of Integrating Capacitors


MODEL 4850 BLOCK DIAGRAM

Model 4850 is a multi-purpose module which can be used as a three mode integrator, a track-and-hold circuit, or as an electronic SPDT switch. Mode control is accomplished by two uncommitted comparators, and external biasing can be introduced for compatibility with digital, analog, or special purpose logic. The comparator input command levels are compatible to many DTL, TTL levels; i.e., reference input may be elevated above common and interchanged respectively for inverse logic commands. The comparators control FET electronic switches that have excellent "feedthrough" characteristics, combined with typical RDS-ON resistances of $20 \Omega$ for the Operate FET switch. The FET switches control the mode condition of the main FET amplifier, and the reset mode condition. A current amplifier drives the main amplifier. Both amplifiers and associated networks are in an internal reset (track) feedback loop. An internal bound circuit improves overdrive recovery with its output available. The operate mode gain configuration range is flexible with a wide integrating capacitor range of $0.001 \mu \mathrm{~F}$ to $10 \mu \mathrm{~F}$. Input impedances in the order of $10^{11} \Omega$ and ultra-low input bias currents in the FET amplifiers contribute to excellent three-mode integrating; low hold delay rates as a track (reset) and hold module. In the gated amplifier mode, the Model 4850 acts as an SPDT switch which can be commanded to select either one of two inputs and amplifier at arbitrary gains.

## OPERATION-THREE-MODE INTEGRATOR

Model 4850 is principally designed to function as a three-mode integrator. Specifically, the module is capable of integrating a signal, holding the integral, and then resetting the output to zero or to some arbitrary initial condition. Operation in the integrate, hold, or reset mode is controlled by the polarity of the Operate FET switch (pin 1) or Reset FET switch (pin 3). During integration, the output of Model 4850 is represented by the following expressions:

$$
E_{0}=-\frac{1}{R_{i} C_{f}} \int_{0}^{f} E_{i} d t+K E_{i c}
$$

where.
$\mathrm{R}_{\mathrm{i}}=$ input resistance
$\mathrm{C}_{\mathrm{f}}=$ integrating capacitance
$\mathrm{E}_{\text {ic }}=$ arbitrary initial value at $+\leqslant 0$
$\mathrm{K}=1$ : if $\mathrm{R}_{\mathrm{ic}}=10 \mathrm{k}$ or $\frac{10 \mathrm{k}, \pm 0.1 \%}{\mathrm{R}_{\mathrm{ic}}}$


## TRACK-AND-HOLD

The Model 4850 is useful as a track-and-hold operator. In this mode, the output tracks the input signal or holds the output value for a particular time. Operation is controlled only by the polarity of the FET switch (pin 3).
During the tracking operation, the output follows the inverse of the input and can be amplified by a constant, K, depending upon the value of the initial condition input resistance, $\mathrm{R}_{\mathrm{ic}}$, which is determined as follows:

$$
\mathrm{R}_{\mathrm{ic}}=\frac{10 \mathrm{k} \pm 0.1 \%}{\mathrm{~K}}
$$

## ELECTRONIC SPDT SWITCH

When the Reset FET switch, internal to Model 4850, is closed it absorbs all of the input current from pin 6. It is possible, therefore, to switch between the two input signals at arbitrary gains and obtain a "chopped" output of the two signals by utilizing this switch as a control.


| ACCURACY | $\pm 0.1 \%$ |
| :---: | :---: |
| INPUT |  |
| Voltage | $\pm 10 \mathrm{~V}$ |
| Impedance | $2 \mathrm{k} \Omega$ to $10 \mathrm{M} \Omega$ |
| OUTPUT | $\pm 10 \mathrm{~V} @ \pm 20 \mathrm{~mA}$ |
| FEEDBACK |  |
| Capacitance | $0.001 \mu \mathrm{~F}$ to $10 \mu \mathrm{~F}$ |
| Resistance | $2 \mathrm{k} \Omega$ to $10 \mathrm{M} \Omega$ |
| STABILITY |  |
| Average Hold Decay Rate at $+25^{\circ} \mathrm{C}$, max. . . . | $\frac{ \pm .06 \mathrm{mV}}{\mathrm{C}(\operatorname{in} \mu \mathrm{~F})}(\max .)$ |
| at $+60^{\circ} \mathrm{C}$, max. | $\frac{ \pm 0.5 \mathrm{mV}}{\mathrm{C}(\text { in } \mu \mathrm{F})} \text { (max.) }$ |
| Output Switching Jump, max. | $\frac{ \pm 0.05 \mathrm{mV}}{\mathrm{C}(\operatorname{in} \mu \mathrm{~F})}(\max .)$ |
| Feedthrough |  |
| Operate FET Switch Open | $\pm 1 \mathrm{mV}$ |
| SWITCHING PERFORMANCE |  |
| Aperture Time | 800 nSec |
| Acquisition Time (Settling to 0.05\%) | $80 \mu \mathrm{Sec}$ |
| MODE CONTROL COMPARATORS |  |
| Minimum Logic Level | $\pm 0.35 \mathrm{~V}$ |
| Maximum Logic Level |  |
| Reference Level |  |
| TEMPERATURE STABILITY |  |
| Operate Mode | $\pm 35 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ (max.) |
| Reset Mode | $\pm 3 \mathrm{mV} /{ }^{\circ} \mathrm{C}$ (max.) |
| TEMPERATURE RANGE | $0^{\circ} \mathrm{C}$ to $+60^{\circ} \mathrm{C}$ |
| POWER REQUIREMENT | $\pm 15 \mathrm{~V}$ @ $\pm 70 \mathrm{~mA}$ |
| CASE Style |  |
| SOCKET .................... | 6024 (\$4.00) |

[^1]
## POWER SUPPLIES



## FEATURES

- Small Size (Encapsulated Modules)
- Short Circuit Protection
- Excellent Line and Load Regulation
- 25 mA to 1000 mA Output Current
- No RFI Generated or Transmitted
- Versatile and Trimmable (Models 2203/2204)
- Custom Modifications Available

Reliable power is the foundation of analog or logic systems. Teledyne Philbrick designs and manufactures a comprehensive line of Power Supplies for logic networks and circuit modules such as operational amplifiers, digital-to-analog and analog-to-digital converters, and nonlinear circuit modules.

HIGH PERFORMANCE

|  | 2203 | 2204 | 2208 | 2209 | 2210 | 2211 | 2212 | 2215 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OUTPUT |  |  |  |  |  |  |  |  |
| Voltage ( $\pm 1 \%$ ) | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ | $\pm 15 \mathrm{~V}$ |
| Current, operating | $\pm 100 \mathrm{~mA}$ | $\pm 50 \mathrm{~mA}$ | $\pm 100 \mathrm{~mA}$ | $\pm 50 \mathrm{~mA}$ | $\pm 25 \mathrm{~mA}$ | $\pm 50 \mathrm{~mA}$ | $\pm 100 \mathrm{~mA}$ | $\pm 200 \mathrm{~mA}$ |
| Current, short circuit | $\pm 60 \mathrm{~mA}$ | $\pm 30 \mathrm{~mA}$ | $\pm 60 \mathrm{~mA}$ | $\pm 30 \mathrm{~mA}$ | $\pm 45 \mathrm{~mA}$ | $\pm 90 \mathrm{~mA}$ | $\pm 140 \mathrm{~mA}$ | $\pm 360 \mathrm{~mA}$ |
| REGULATION |  |  |  |  |  |  |  |  |
| Line, max. (105-125 Vac) | $\pm 0.03 \%$ | $\pm 0.03 \%$ | $\pm 0.03 \%$ | $\pm 0.03 \%$ | $\pm 0.2 \%$ | $\pm 0.1 \%$ | $\pm 0.05 \%$ | $\pm 0.02 \%$ |
| Load, max (0-100\%) | $\pm 0.03 \%$ | $\pm 0.015 \%$ | $\pm 0.03 \%$ | $\pm 0.015 \%$ | $\pm 0.2 \%$ | $\pm 0.1 \%$ | $\pm 0.1 \%$ | $\pm 0.05 \%$ |
| Temperature coefficient, max. | $\pm 0.01 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.01 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.01 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.01 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.02 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.015 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.015 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.02 \% /{ }^{\circ} \mathrm{C}$ |
| Warm-up drift | 45 mV | 35 mV | 45 mV | 35 mV | 30 mV | 35 mV | 45 mV | 45 mV |
| Ripple and noise, max. | 1 mV rms | 1 mV rms | 1 mV rms | 1 mV rms | 1 mV rms | 1 mV rms | 1 mV rms | 1 mV rms |
| Impedance @ 10 kHz | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ |
| TEMPERATURE RANGE |  |  |  |  |  |  |  |  |
| Operating ( ${ }^{\circ} \mathrm{C}$ ) | -25 to +85 | -25 to +85 | -25 to +85 | -25 to +85 | 0 to +70 | 0 to +70 | 0 to +70 | 0 to +70 |
| Storage ( ${ }^{\circ} \mathrm{C}$ ) | -35 to +125 | -35 to +125 | -35 to +125 | -35 to +125 | -25 to +85 | -25 to +85 | -25 to +85 | -25 to +85 |
| INPUT |  |  |  |  |  |  |  |  |
| Voltage ( $\pm 10 \%$ ) | 115/230 Vac | 115/230 Vac | 115 Vac | 115 Vac | 115 Vac | 115 Vac | 115 Vac | 115 Vac |
| Isolation | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ |
| Frequency ( Hz ) | 50 to 400 | 50 to 400 | 50 to 400 | 50 to 400 | 50 to 400 | 50 to 400 | 50 to 400 | 50 to 400 |
| Case Style (See page 63) | C1 | C1 | C3 | C3 | C4 | C4 | C3 | C5 |
| Mating Socket (See page 68) | 6036 | 6036 | 6036 | 6036 | 6036 | 6036 | 6036 | 6036 |
| Options* | -- | -- | 21 | 21 | 21 | 21 | 21 | 221521 |

* Options Available

For $230 \mathrm{Vac}, 50-400 \mathrm{~Hz}$ input, add the suffix " 21 " to the model number. No additional charge.

All power supplies are complete and self-contained. No external transformers or filters are required for stable, accurate operation. This one unit construction is easier to use, and reduces component and assembly costs of the equipment being manufactured. For added mechanical strength the encapsulated supplies can be fastened to a P.C. Board or in optional mating sockets by supplied holddown nut.

## PROTECTION

All Teledyne Philbrick power supplies are protected against overheating from direct short circuits to ground. The dual supplies will track each other so that a short on one output will automatically reduce the other output to prevent damage to the load circuitry.

## LOW COST

2216
2217
MICROLOGIC
HI POWER
2206
2213
2207

| $\pm 26 \mathrm{~V}$ | $\pm 120 \mathrm{~V}$ | +5 V | +5 V | $\pm 15 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- | :--- |
| $\pm 45 \mathrm{~mA}$ | $\pm 40 \mathrm{~mA}$ | +500 mA | +1000 mA | $\pm 500 \mathrm{~mA}$ |
| $\pm 60 \mathrm{~mA}$ | $\pm 75 \mathrm{~mA}$ | +150 mA | +1.2 Amp | $\pm 150 \mathrm{~mA}$ |


| $\pm 0.05 \%$ | $\pm 0.01 \%$ | $\pm 0.1 \%$ | $\pm 0.05 \%$ | $\pm 0.02 \%$ |
| :--- | :--- | :--- | :--- | :--- |
| $\pm 0.05 \%$ | $\pm 0.01 \%$ | $\pm 0.15 \%$ | $\pm 0.1 \%$ | $\pm 0.05 \%$ |
| $\pm 0.02 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.05 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.01 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.02 \% /{ }^{\circ} \mathrm{C}$ | $\pm 0.03 \% /{ }^{\circ} \mathrm{C}$ |
| 35 mV | -- | 15 mV | 25 mV | 25 mV |
| 1 mV rms | 2 mV rms | 2 mV p-p | 1 mV rms | $5 \mathrm{mV} \mathrm{p}-\mathrm{p}$ |
| $0.2 \Omega$ | $0.8 \Omega$ | $0.1 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ |


| 0 to +70 | 0 to +70 | -25 to +85 | -25 to +70 | -20 to +50 |
| :--- | :--- | :--- | :--- | :--- |
| -25 to +85 | -25 to +85 | -35 to +125 | -55 to +85 | -40 to +75 |


| 115 Vac | 115 Vac | $115 / 230 \mathrm{Vac}$ | 115 Vac | 115 Vac |
| :--- | :--- | :--- | :--- | :--- |
| $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $50 \mathrm{M} \Omega$ | $100 \mathrm{M} \Omega$ |
| 50 to 400 | 50 to 400 | 50 to 400 | 50 to 400 | 50 to 400 |
| C 5 | C 6 | C 1 | C 5 | C 2 |
| 6036 | 6036 | 6036 | 6036 | -- |
| 221621 | 221721 | - | 21 | 21 |



## SERIES OPERATION

For applications where higher supply voltages are needed, these power supplies can be operated single ended and stacked as shown in Figure 1. The worst case regulation now would be the sum of the individual supplies, no tracking. The break-down voltage in this type of application is approximately $\pm 400$ volts.


## GROUNDING PROCEDURES

Power supply grounding is one of the most important factors in powering analog loads. Very often system design problems can be avoided or completely eliminated by following good grounding procedures.
We recommend that all ground points be tied together at a single point to minimize the noise and excessive ground currents caused by differences in ground potential. These connections should be as short as possible impedance.


## TRIMMING

Models 2203 and 2204 have trim terminals which allow adjustment of the output voltage from $\pm 14.5$ to $\pm 15.5$ Vdc . The trimming hookup is given below.


[^2]
## MECHANICAL SPECIFICATIONS

All dimensions in parentheses are expressed in centimeters.
Unless otherwise specified, module pins are 0.04 (0.10) diameter and are spaced
0.20 ( 0.51 ) apart. Spacing between rows of pins is 0.80 (2.03).

LINEAR and NONLINEAR PRODUCTS








|  | 6128 | 6129 <br> BOARD THICKNESS: 0.09 (0.23) EPOXY OVERALL HEIGHT: 0.50 (1.27) |
| :---: | :---: | :---: |
| NSK-9 <br> BOARD THICKNESS: $0.09(0.23)$ EPOXY <br> OVERALL HEIGHT: $0.68(1.73)$ | NSK-13 | NSK-14 <br> BOARD THICKNESS: 0.09 (0.23) EPOXY OVERALL HEIGHT: 0.68 (1.73) |
| NSK-20 | US-PP <br> BOARD THICKNESS: $0.125(0.318)$ EPOXY <br> OVERALL HEIGHT: 0.43 (1.08) |  |

## Standard Products still available, not recommended for New Designs.

| 1003 | FET, High CMRR, Low Drift | 1408 | FET, Economy, Epoxy | Q25AH | FET, High Reliability, TO-8 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 0 0 3 0 1}$ | FET, High CMRR, Low Drift | 140801 | FET, Economy, Epoxy | Q200 | Micropower |
| $\mathbf{1 0 0 9}$ | FET, General Purpose | 140802 | FET, Economy, Epoxy | QFT-2 | FET, General Purpose |
| 100901 | FET, General Purpose | 140810 | FET, Economy, TO-8 | QFT-2A | FET, General Purpose |
| 100902 | FET, General Purpose | 140811 | FET, Economy, TO-8 | QFT-2B | FET, General Purpose |
| 1011 | FET, Fast Differential | 140812 | FET, Economy, TO-8 | SA-1 | High Performance |
| 101101 | FET, Fast Differential | P2A | Premium, Parametric | SA-2 | High Performance |
| 101102 | FET, Fast Differential | P65AU | General Purpose | SA-3A | High Performance |
| 1018 | Low Drift, Differential | P85AU | High Performance | SP2A | Premium Parametric |
| 101801 | Low Drift, Differential | PP45 | Fast Inverting | SP2AU | Economy Parametric |
| 101802 | Low Drift, Differential | PP45U | Fast Inverting | SQ-3 | High Input Impedance |
| 101803 | Low Drift, Differential | PP65A | High Reliability, General Purpose | SQ-10A | General Purpose |
| 101804 | Low Drift, Differential | PP65AU | General Purpose |  |  |
| $\mathbf{1 0 1 9}$ | FET, Fast Differential | PP85AU | High Performance |  |  |


| Modular Op Amps |  |  |
| :---: | :---: | :---: |
| 1005 | 20 V Output | 22 |
| 1006 | FET, Micropower | 22 |
| 1008 | FET, $10 \mathrm{~V} / 30 \mathrm{~mA}$ Output | 22 |
| 1016 | High Speed, 100 mA Output | 22 |
| 1017 | Economy, High Power | 22 |
| 1020 | Low Drift, Differential, $5.0 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 18 |
| 102001 | Low Drift, Differential, $1.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 18 |
| 102002 | Low Drift, Differential, $0.5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 18 |
| 102003 | Low Drift, Differential, $0.25 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 18 |
| 1021 | FET, High CMRR | 16 |
| 1022 | FET, 140 V Output | 22 |
| 1023 | FET, Low Drift, $5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 18 |
| 102301 | FET, Low Drift, $2 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 18 |
| 1024 | Economy, 20 mA Output | 14 |
| 1025 | FET, Fast Settling | 20 |
| 1026 | FET, General Purpose, $50 \mathrm{pA}, 50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 16 |
| 102601 | FET, General Purpose, $20 \mathrm{pA}, 20 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 16 |
| 102602 | FET, General Purpose, $10 \mathrm{pA}, 20 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 16 |
| 1027 | FET, Fast Differential, $50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 20 |
| 102701 | FET, Fast Differential, $15 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ | 20 |
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[^0]:    (1) Accuracy as a \% of full scale includes gain, offset and linearity errors.
    (2) Includes both phase shift and amplitude errors, measured at peak of 10 V Triangle wave input

[^1]:    1. Specifications are typical at $+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{cc}} @ \pm 15 \mathrm{~V}$, unless otherwise indicated.
[^2]:    Characteristics typical at $25^{\circ} \mathrm{C}$ with nominal line voltage, unless otherwise indicated.

